# Multi-objective Power Flow Optimization Based on Improved Hybrid Crow Search Algorithm: A Novel Approach 

Gonggui Chen, Xiang Wang, Shuangjin Mo, Jian Zhang, Wei Xiong, Hongyu Long* and Mi Zou


#### Abstract

An improved hybrid crow search algorithm (IHCSA), whose purpose is to find the best measured solution (BMS), is proposed to solve the multi-objective optimal power flow (MOOPF) problem. The proposed IHCSA, which creatively combines the advanced ideas and strategies of sinusoidal nonlinear dynamic transformation awareness probability (SNDTAP) and tent map switching fly length (TMSFL), introducing the mutation and crossover processes of differential evolution (DE), obtains a better BMS. Three innovative optimization strategies are integrated into this paper. The proposed screening approach of Pareto-priority mechanism (SAPM) ensures that the state variables meet the inequality constraints of power systems. The Pareto optimal set (POS) is obtained by elite non-dominant sorting method (ENSM). Besides, the BMS, obtained by fuzzy membership theory, is filtered from POS. For practical purposes, five objective functions are considered. Three various scale test systems are applied to validate the performance of the IHCSA. Simulation results reveal that the proposed method has a greater competitive advantage in addressing non-convex MOOPF problems of different scales. In addition, Hypervolume (HV) and Spacing (SP) are used to quantitatively evaluate the diversity and consistency of POS gained by IHCSA. The evaluation results prove that the proposed approach has excellent performance and great application prospects.


Index Terms-Improved hybrid CSA, optimal power flow, optimization strategies, performance evaluation indexes

Manuscript received May 25, 2022; revised September 23, 2022. This work was supported by the National Natural Science Foundation of China (52007022), the Project funded by the China Postdoctoral Science Foundation(2021M693930).

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## I. INTRODUCTION

OPTIMAL power flow (OPF), an optimization technique that has received extensive attention in power system research., must ensure the safety of the system operation when adjusting control variables and meet the physical constraints simultaneously. The purpose is to obtain an ideal operation state for the system[1]. The crux of the matter is that OPF cannot be put into a continuous mathematical model for the solution, which is one of the several difficulties in practical engineering projects[2].

Since the 21 st century, the use of electric energy has been further enhanced, and the task of the electric power system has become more onerous. How to better plan and optimize the electric power system has attracted the attention of researchers[3,4]. In previous studies, the OPF problem is mainly concerned with minimizing fuel cost, emission, and active power loss, respectively. To measure the running state of the power system comprehensively and meet the needs of the actual system, the research often considers multiple optimization objectives in an integrated manner. The multi-objective uncoordinated constraint problem in the power system is called the multi-objective optimal power flow problem (MOOPF)[5].

The MOOPF problem, which has non-convex and high dimensional characteristics, optimizes the given targets by tailoring the control variables to meet various constraints. Unlike the search for a single optimal decision, the MOOPF attempts to calculate a set of control schemes, and, ultimately, the best-measured solution (BMS).

Previously, classical methods were to assign different weights to each objective in dealing with the MOOPF problem based on decision-makers' priorities and solutions. However, traditional methods also inevitably have some defects. For example, the conventional approach is not suitable for the unknown situation of decision-makers. For high-dimensional problems such as MOOPF, it is almost impossible to find POS in a complex system[6]. Therefore, the use of other feasible ways to deal with the MOOPF problem deserves to be developed vigorously[7-11].

Throughout the years, breakthroughs and innovations in computer technology have provided a solid foundation for the growth of heuristic algorithms lately[12-19]. Many researchers have made much progress in solving the MOOPF problem with heuristic algorithms[20-23]. For instance, BP neural network is introduced to predict the latent schemes around BMS [24]. A method called Manta ray foraging optimization is used to find feasible solution
sets[25]. In literature [26], a multi-objective optimizer NSWOA was applied to multiple engineering problems. In literature [27], a dimension-based firefly algorithm obtains POS with high-quality effects. A hybrid firefly-bat algorithm is introduced to enhance the population diversity in [28]. The modified beetle antennae search algorithm and BP are applied to solve the MOOPF problem in [29]. In literature [30], a multi-objective optimization approach is introduced to resource management of heterogeneous cellular networks. The results reveal that applying the heuristic algorithm to solve the MOOPF problem is very effective.

Crow search algorithm (CSA) is a new intelligent optimization algorithm developed recently. It was proposed by Askarzadeh in 2016[31]. Due to its relatively simple structure and few key parameters, CSA has been widely used in different fields[32-36]. Nevertheless, the original CSA is still prone to fall into local optimization and lack diversity[37].
In order to solve the MOOPF problem, this paper proposes an improved hybrid crow search algorithm (IHCSA) with sinusoidal nonlinear dynamic switching awareness probability and tent map switching flight length, combined with the variation and crossover process model of the differential evolution (DE) algorithm. To evaluate the practicability of IHCSA, several research cases were selected to test it on IEEE30-, 57-, and IEEE118-bus systems and the test results are more accurate than those of recent literature, highlighting IHCSA's applicability and core competencies.

The rest of article is structured as follows: The mathematical model in the area of MOOPF is depicted in Section II. The strategies to solve the MOOPF problem are given in Section III. The IHCSA's application in MOOPF is described at Section IV. In addition, Section V represents simulation study and scenario analysis of ten different research components. Finally, the performance evaluation index data are obtained at Section VI. Section VII summarizes this work.

## II. Moopf Mathematical Model

The MOOPF problem model contains the examination and optimization of different combinations of objectives. At the same time, various constraints of the system must be included in the scope of restrictions[38]. The components of the MOOPF mathematical model are described in detail as the following:

$$
\begin{gather*}
\operatorname{Min} S_{o b j}(x, u)=\left\{S_{1}(x, u), \cdots, S_{i}(x, u), \cdots, S_{m}(x, u)\right\}  \tag{1}\\
H_{k}(x, u)=0, \quad k=1, \cdots, k, \cdots, H_{\text {length }}  \tag{2}\\
G_{j}(x, u) \leq 0, \quad j=1, \cdots, j, \cdots, G_{\text {length }} \tag{3}
\end{gather*}
$$

where $S_{i}(x, u)$ represents the $i$ th objective function that needs to be optimized, and $m$ is the target number. $H_{k}(x, u)$ denotes the $k$ th equality constraint and $G_{j}(x, u)$ describes the $j$ th inequality constraint. $H_{\text {length }}$ and $G_{\text {length }}$ depict the amount of equality restraints and inequality restraints, separately.
$x^{T}=\left[P_{G e n 1}, V_{L 1}, \cdots, V_{L C_{P Q}}, Q_{G e n 1}, \cdots, Q_{\text {GenN }_{G}}, S_{T L_{1}}, \cdots, S_{T L_{C r L}}\right]$
where $x$ is defined as the vector of state variables, which incorporates a large variety of variables. Active power output of generator at slack bus $P_{\text {Gen } 1}$, which regulates the
system output. $V_{L}$, load bus voltage, must not cross the line voltage carrying range. Generator reactive power $Q_{G e n}$, which cannot be ignored. The apparent power of transmission line $S_{T L}$ is also in the scope of consideration.
$u$ is a vector of control variables, which incorporates many control points. The tap setting of the transformers $T$ is considered. Active power output of generators other than $P_{G e n 1}$, is the main source of energy for the system. The voltage magnitude of generators $V_{G e n}$, reflects, to some extent, the generator operating condition. The injected reactive power of shunt compensators $Q_{C}$, enables the system network to work better. It can be described as:
$u^{T}=\left[P_{\text {Gen2 } 2}, \cdots, P_{\text {GenN }_{G}}, V_{\text {Gen } 1}, \cdots, V_{\text {GenN }}, T_{1}, \cdots, T_{N_{T}}, Q_{C_{1}}, \cdots, Q_{C_{N_{C}}}\right]$
where $C_{P Q}$ signifies the count of load buses, and $N_{G}$ depicts the number of generators. CTL is the count of transmission lines. $N_{T}$ and $N_{C}$ denote the number of transformers and shunt compensators.

## A. Objective Functions

This paper will optimize the five objective functions, including basic fuel cost, fuel cost with value-point, emission, voltage deviation, and active power loss. The specific groups can be seen in TABLE II.

$$
\begin{align*}
& \text { 1) } S_{\text {fcost }} \\
& \qquad S_{\text {fcost }}=\sum_{i=1}^{N_{\text {Gem }}}\left(C a_{i}+C b_{i} P_{\text {Geni }}+C d_{i} P_{\text {Geni }}^{2}\right) \$ / \mathrm{h} \tag{6}
\end{align*}
$$

where $S_{\text {fcost }}$, basic fuel cost, depicts one of the main costs. $C a_{i}, C b_{i}$ and $C d_{i}$ are the cost coefficients.
2) $S_{\text {emission }}$
$S_{\text {enission }}=\sum_{i=1}^{N_{\text {Gen }}}\left[\alpha_{i} P_{\text {Geni }}^{2}+\beta_{i} P_{\text {Geni }}+\zeta_{i}+\eta_{i} \exp \left(\lambda_{i} P_{\text {Geni }}\right)\right]$ ton $/ \mathrm{h}$
where $S_{\text {emission }}$ represents the total emissions. $\alpha_{i}, \beta_{i}, \gamma_{i}, \zeta_{i}$, and $\lambda_{i}$, emission factors, are some real numbers.
3) $S_{\text {Ploss }}$

$$
\begin{equation*}
S_{\text {Ploss }}=\sum_{k=1}^{N_{T M}} G_{k}\left[V_{i}^{2}+V_{j}^{2}-2 V_{i} V_{j} \cos \left(\delta_{i}-\delta_{j}\right)\right] \mathrm{MW} \tag{8}
\end{equation*}
$$

where $S_{\text {Ploss }}$ depicts the active power loss. $G_{k}$ depicts the conductance of branch $k . V_{i}$ and $V_{j}$ refer to the voltage magnitude at bus $i$ and $j . \delta_{i}$ and $\delta_{j}$ describe voltage angle at bus $i$ and $j$, respectively.
4) $S_{\text {fcost_vp }}$

$$
\begin{align*}
& S_{\text {fcost-vp }}=\sum_{i=1}^{N_{G}}\left[a_{i}+b_{i} P_{\text {Gen }_{i}}+c_{i} P_{\text {Geni }}^{2}+\right.  \tag{9}\\
& \left.\left|d_{i} \sin \left(e_{i}\left(P_{\text {Geni }}^{\min }-P_{\text {Geni }}\right)\right)\right|\right] \$ / \mathrm{h}
\end{align*}
$$

where $S_{\text {fost_vp }}$ depicts the fuel cost with value-point loadings. $d_{i}$ and $e_{i}$ depict cost coefficients. $P_{\text {Geni }}^{\min }$ denotes lower active power, which is valid for the $i$ th generator.
5) $S_{V D}$

Voltage deviation reflects the quality of the electrical energy in the line and its magnitude directly influences the power system's stability and economic benefit. It can be written as below:

$$
\begin{equation*}
S_{V D}=\sum_{n u=1}^{N_{P Q}}\left|V_{n u}-1\right| \tag{10}
\end{equation*}
$$

where $S_{V D}$ denotes the total voltage deviation of a system.

## B. Variable Constraints

Only when the power system's all constraints are satisfied simultaneously does the optimization of five objective functions have practical significance.

## 1) Equality Constraints

The equality constraints reveal elegantly load flow equations, whose connotations are depicted below:
$P_{G i}=P_{D i}+V_{i} \sum_{j=1}^{N b_{i}} V_{j}\left(G_{i j} \cos \left(\delta_{i}-\delta_{j}\right)+B_{i j} \sin \left(\delta_{i}-\delta_{j}\right)\right), \forall i \in N B$
$Q_{G i}=Q_{D i}+V_{i} \sum_{j=1}^{N b_{i}} V_{j}\left(G_{i j} \sin \left(\delta_{i}-\delta_{j}\right)-B_{i j} \cos \left(\delta_{i}-\delta_{\mathrm{j}}\right)\right), \forall \mathrm{i} \in N_{P Q}$
where $P_{G i}$ and $Q_{G i}$ denote the injected active and reactive power at generator bus $i$ while $P_{D i}$ and $Q_{D i}$ depict the active and reactive load demand at load bus $i$. In addition, $G_{i j}$ and $B_{i j}$ signify the conductance and susceptance, respectively. $N b_{i}$ depicts the count of the buses contiguous with bus $i$, including bus $i ; N B$ is the amount of system buses other than the slack bus; $N_{P Q}$ indicates the amount of PQ buses.

## 2) Inequality Constraints

System variables need to be restricted to valid ranges, inequality constraints involve constraints of state variables and control ones[28].
(1) Inequality constraints of control variables
(i) Active Power $P_{G}$ Constraints

$$
\begin{align*}
& P_{\text {Geni }}^{\max }-P_{\text {Geni }} \geq 0  \tag{13}\\
& P_{\text {Geni }}-P_{\text {Geni }}^{\min } \geq 0
\end{align*}, i \in N_{G}(i \neq 1)
$$

(ii) Voltage $V_{G}$ Constraints

$$
\begin{align*}
& V_{\text {Geni }}^{\max }-V_{\text {Geni }} \geq 0 \\
& V_{\text {Geni }}-V_{\text {Geni }}^{\min } \geq 0 \tag{14}
\end{align*}, i \in N_{G}
$$

(iii) Transformer Tap-settings $T$ Constraints

$$
\begin{align*}
& T_{i}^{\max }-T_{i} \geq 0  \tag{15}\\
& T_{i}-T_{i}^{\min } \geq 0
\end{align*}, i \in N_{T}
$$

(iv) Reactive Power Sources $Q_{C}$ Constraints

$$
\begin{align*}
& Q_{C i}^{\max }-Q_{C i} \geq 0  \tag{16}\\
& Q_{C i}-Q_{C i}^{\min } \geq 0
\end{align*}, i \in N_{C}
$$

(2) Inequality constraints of state variables
(i) limitations for $P_{G e n 1}$

$$
\begin{align*}
& P_{G e n 1}^{\max }-P_{G e n 1} \geq 0 \\
& P_{\text {Gen } 1}-P_{G e n 1}^{\min } \geq 0 \tag{17}
\end{align*}
$$

(ii) restrictions on voltages at load buses

$$
\begin{align*}
& V_{L i}^{\max }-V_{L i} \geq 0  \tag{18}\\
& V_{L i}-V_{L i}^{\min } \geq 0
\end{align*}, i \in N_{P Q}
$$

(iii) restrictions on generator reactive power

$$
\begin{align*}
& Q_{\text {Geni }}^{\max }-Q_{\text {Geni }} \geq 0  \tag{19}\\
& Q_{\text {Geni }}-Q_{\text {Geni }}^{\min } \geq 0
\end{align*}, i \in N_{G}
$$

(iv) restrictions on apparent power

$$
\begin{equation*}
S_{i j}^{\max }-S_{i j} \geq 0, i j \in N_{T L} \tag{20}
\end{equation*}
$$

## III. Multi-objective Problem Processing Strategy

In order to choose the most suitable BMS for the current situation among many alternatives, three multi-objective strategies are taken into adoption.

## A. Constrained Preemptive Strategy

It can be obtained from the Newton-Raphson power flow calculation whether the $i$ th individual violates the equality constraints. Moreover, the control variables of the $i$ th crow could be depicted in (21).

$$
u_{i}= \begin{cases}u_{i}^{\max } & \text { if } u_{i}>u_{i}^{\max }  \tag{21}\\ u_{i}^{\min } & \text { if } u_{i}<u_{i}^{\min } \\ u_{i} & \text { otherwise }\end{cases}
$$

Given the inequality constraint treatment of state variables, a screening approach of the Pareto-priority mechanism (SAPM), which is significantly different from the traditional penalty coefficient method, is proposed to solve this problem. Its main steps are as follows:
(i) Calculate the violation of inequality constraints for $i$ th individual $\operatorname{viol}\left(u_{i}\right)$ (22).

$$
\begin{equation*}
\operatorname{sum} \_\operatorname{viol}\left(u_{i}\right)=\sum_{j=1}^{H_{s}} \max \left(G_{j}\left(x, u_{i}\right), 0\right) \tag{22}
\end{equation*}
$$

where $H_{S}$ represents the count of inequality constraints on the state variables.
(ii) $u_{1}$ and $u_{2}$, two different control variables, are selected randomly, and their violations are compared. When the formula (23) is satisfied, $u_{1}$ is dominant $u_{2}$.

$$
\begin{equation*}
\operatorname{sum}]_{-} \operatorname{viol}\left(u_{1}\right)<\text { sum_viol }\left(u_{2}\right) \tag{23}
\end{equation*}
$$

(iii) If any of the conditions (24) and (25) are satisfied, it means that $u_{1}$ is dominant $u_{2} . u_{1}$ is regarded as a Pareto non-dominated solution.

$$
\begin{gather*}
\operatorname{sum_{-}} \operatorname{viol}\left(u_{1}\right)=\operatorname{sum}_{-} \operatorname{viol}\left(u_{2}\right)  \tag{24}\\
\left\{\begin{array}{l}
S_{i}\left(x, u_{1}\right) \leq S_{i}\left(x, u_{2}\right), \quad \forall i \in\{1,2, \ldots, m\} \\
S_{j}\left(x, u_{1}\right)<S_{j}\left(x, u_{2}\right), \quad \exists j \in\{1,2, \ldots, m\}
\end{array}\right. \tag{25}
\end{gather*}
$$

## B. Elite Non-dominated Sorting Method

To obtain the uniformly distributed Pareto front, this paper adopts an elitist non-dominated ranking method first proposed by Deb in 2002[39]. The proposed Pareto dominant rule determines two attributes of each individual.

## C. Rank and Density Calculation

1) Rank

It is assumed that each crow individual $i$ in the crow population has two parameters: $C_{o}(i)$ and $C_{m}(i) . C_{o}(i)$ depicts the amounts of crows dominated crow $i$, and $C_{m}(i)$ represents the number of individuals dominated by individual $i$. The rules for determining the rank are described as follows:

Step1: Find all crows $i$ with $C_{o}(i)=0$, place them in set $P$, and mark them as Rank=1.

Step2: For each individual crow $k$ in the current set $P$, we probe into the number of crow individual $C_{m}(k)$ it dominated. If $C_{o}(k)=1$, then we put crow individual $k$ into another set $Q$, and mark them as Rank=2.
Step3: Repeat step1 and step2 until all crows have their rank.

## 2) Density Calculation

Evaluation of a collection of multiple programs, the crowding distance, can be obtained by calculating the average distance between each adjacent two positions in the collection.

Density Calculation of the $i$ th crow can be defined as
below:

$$
\begin{equation*}
D_{\text {calculation }}(i)=\sum_{j=1}^{N S} \frac{S_{j}(i-1)-S_{j}(i+1)}{S_{j}^{\max }-S_{j}^{\min }} \tag{26}
\end{equation*}
$$

where $N S$ is the number of objective functions. In addition, $S_{j}^{\max }$ and $S_{j}^{\text {min }}$ indicate the $j$ th goal's upper and lower boundary values.

It is used to distinguish the order between multiple Pareto solutions in the same hierarchy, with the solution with the highest number being considered the manager's preferred solution. This is because solutions with larger values are more applicable.

## D. Best-Measured Solution Based on Fuzzy Affiliation Rule

We are able to obtain multiple solutions with the same priority by the previous method, but we cannot objectively select from them the individual that is applicable at a given moment. A solution, which is determined quickly and objectively and meets the scheduler's current requirements, is called the best-measured solution (BMS).

The following two formulas describe in detail the basis for BMS selection. $F_{i, k}$ depicts satisfaction of the $i$ th goal for the $k$ th crow.

$$
\begin{gather*}
F_{i, k}=\left\{\begin{array}{cc}
1 & S_{i} \leq S_{i}^{\min } \\
\frac{S_{\text {max }}-S_{i}}{S_{i}^{\text {max }}-S_{i}^{\text {min }}} & S_{i}^{\min }<S_{i}<S_{i}^{\max } \\
0 & S_{i} \geq S_{i}^{\max }
\end{array}\right.  \tag{27}\\
i=1,2, \ldots N S \\
k=1,2, \ldots, N P  \tag{28}\\
\operatorname{Sat}(k)=\frac{\sum_{i=1}^{N S} F_{i}(k)}{\sum_{k=1}^{N P} \sum_{i=1}^{N S} F_{i}(k)}
\end{gather*}
$$

where the $\operatorname{Sat}(k)$ represents the superiority of the $k$ th solution, the BMS achieved by the rule has the highest satisfaction. $N P$ is the size of POS.

## IV. Improved and Hybrid Approach

The original crow search algorithm only has two main parameters, awareness probability (AP) and flight length (fl), which are simple and flexible. It has been applied to many interesting areas and projects.

However, the original CSA is still prone to fall into local optimization and lacks enough diversity. An improved hybrid crow search algorithm is proposed to aim at the above shortcomings.

## A. Standard Crow Search Algorithm

The crow search algorithm was proposed by Askarzadeh in 2016 and applied to engineering design problems[31]. It is a new optimization algorithm proposed by imitating the intelligent behavior of crows when they store and steal food.

The search process of the crow search algorithm is controlled by two parameters: awareness probability (AP) and flight length $(f l)$. If the random number rand is bigger than $A P$, the crow is closer to the memory location of the hidden food. Otherwise, the crow will choose a random location in the search space to deceive the stalker. The formula can describe the search process(29):
$C_{i}(k+1)=\left\{\begin{array}{l}C_{i}(k)+r_{j} \times f l(k) \times\left(M_{j}(k)-C_{i}(k)\right) \text { if } r_{i} \geq A P_{j} \\ \text { a rand position } \quad \text { otherwise }\end{array}\right.$
where $C_{i}(k)$ is the position of crow $i$ at iteration $k . M_{j}(k)$ is crow $j$ 's memory of hiding food location at the current iteration. $r_{i}$ and $r_{j}$ are two stochastic data in $[0,1] . A P_{j}$ is the awareness probability of crow $j$. Related research clearly depicts that $f l$ works for most problems when it is 2 .

## B. The IHCSA

Three methods are proposed to amend the standard CSA, SNDTAP, TMSFL and SAPM.

1) Sinusoidal Nonlinear Dynamic Transforming Awareness Probability

For the normative CSA, Askarzadeh believes it can achieve strong applicability and processing accuracy when $A P$ is 0.1 . However, some researches reveal that sinusoidal nonlinear dynamic switching awareness probability. SNDTAP is proposed to makes $A P$ more dynamic and effective, which could be defined as below:

$$
\begin{equation*}
A P=A P_{\min }+\left(A P_{\max }-A P_{\min }\right) \sin \left(\frac{\pi}{2} \frac{k}{K_{\max }}\right) \tag{30}
\end{equation*}
$$

where $A P_{\text {max }}$ and $A P_{\text {min }}$ are set as 0.5 and 0.01 , representing the maximum and minimum values of awareness probability, respectively.

## 2) Tent Map Switching Fly Length

$f l$ is usually set as 2 in the standard CSA. According to the algorithm's principle, $f l$ will affect the flight distance of crows, affecting the global search and local search ability of CSA. To improve the global and regional random traversal capability of the algorithm search, the tent map method is introduced to make $f l$ switch dynamically along with the iterative process, and its transformation process can be understood as follows:

$$
f l(k+1)=\left\{\begin{array}{l}
\frac{f l(k)}{\alpha} f l(k)<\alpha  \tag{31}\\
\frac{1-f l(k)}{1-\alpha} \quad f l(k) \geq \alpha
\end{array} \quad \alpha \in(0,1)\right.
$$

where $f l(k)$ represents the size when the number of iterations is $k$. As shown in the literature [37], $\alpha$ is set as 0.7 .
3) Mutation and Crossover Operation of DE

The crow search algorithm cooperates with global and local search. The mutation crossover mechanism of the DE algorithm is embedded in CSA method, which improves the CSA's ability to jump out of local optimal and enhances the diversity of the original crow search algorithm.

Meanwhile, it is also helpful to improve its local search capability of CSA. The mutation updating way of DE algorithm is as below:

$$
\begin{align*}
& M_{-} C(k+1)=C_{r 1}(k)+F_{c}\left(C_{r 2}(k)-C_{r 3}(k)\right) \\
& r_{i} \in[1, N P] \quad i=1,2,3 \tag{32}
\end{align*}
$$

where $M_{-} C(k+1)$ is a new crow created by a mutation mechanism. $C_{r 1}, C_{r 2}$, and $C_{r 3}$ are the three crows randomly selected from the crow population in the current iteration. $r_{1}$, $r_{2}$, and $r_{3}$ are three different random numbers. $F_{c}$, a fundamental constant, denotes a variable scaling factor that controls the variation process.

The search and update approach corresponding to the crossover process is as below:
$C_{i, d}(k+1)= \begin{cases}M_{-} C_{i, d}(k+1), & \text { if } \operatorname{rand}(0,1) \leq C R \text { or } d=d_{\text {rand }} \\ C_{i, d}(k), & \text { otherwise }\end{cases}$

$$
\begin{equation*}
d=1, \cdots, d, \cdots, D_{c v} \tag{33}
\end{equation*}
$$

where, $D_{c v}$ represent the dimensions of control variables. $d$ depicts $d$-th control variables. Besides, $C R$, the crossover factor, usually doesn't exceed 1 . It's a real constant. $D_{\text {rand }}$ is a random number from 1 to $D_{c v}$.

The pseudo-code of IHCSA is succinctly described in TABLE I.

TABLE I
PSEUDO CODE OF IHCSA

```
Input: }\mp@subsup{S}{obj}{}(x,u)={\mp@subsup{S}{1}{}(x,u),\ldots,\mp@subsup{S}{i}{}(x,u),\ldots,\mp@subsup{S}{m}{}(x,u),
            The crow group is stochastically initialized. under system
constraints. Set relevant parameters of the IHCSA algorithm: crow
population NP, awareness probability }AP\mathrm{ , flight length }fl\mathrm{ , maximum
iteration }\mp@subsup{K}{\mathrm{ max }}{}\mathrm{ , etc.
Begin
    k=0;
    while ( }k<\mp@subsup{K}{\mathrm{ max }}{}\mathrm{ )
    Dynamically update AP by formula (30);
    fl is updated randomly by formula (31);
        for ith crow (i=1,\ldots,Na)
Generate two random numbers named rand1 and rand2.
            if rand 1>AP
                    According to the formula (29) and (32), a global jump search is
performed;
            else
                    for j=1,2,\ldots,N}\mp@subsup{N}{CV}{}\mathrm{ (The dimension of crow individual)
                        if rand 2<CR |d<d
                        Update the j}\mathrm{ -th position of crow }i\mathrm{ according to the formula
(33);
                end
            end
            end
        end
    Renovate the optimal global information;
    k++;
    end
End
output: BMS and Other alternatives;
```


## V. Simulation Result

To validate IHCSA's processing capabilities., the way's performance was tested in IEEE30-, IEEE57-, and IEEE118-bus systems. TABLE II lists ten different cases which need to be handled.
The steps of the MOOPF problem with the IHCSA method are illustrated in Fig. 3. Also, basic codes of three optimization ways are implemented in MATLAB R2019a software in a PC with $\operatorname{Intel}(\mathrm{R})$ Core (TM) i5-7400CPU $@ 3.00 \mathrm{GHz}$ with 16 GB RAM.

## A. Test Systems

An IEEE30-bus system, whose structure is shown in Fig. 1. The main parameters include 6 generators and 30 buses. The upper and lower limitations of taps of 4 transformers are 1.1 p.u. and 0.9 p.u.

Detailed data on the correlation coefficient could be obtained in [28]. The generators and load buses are given,
whose voltage variation ranges are 0.95 to 1.1 p.u.
Does Fig. 2 describes the main features of the IEEE57-bus system, whose detailed data are given in the literature $[27,28]$.

Transformer taps are between 0.9 and 1.1 p.u, shunt capacitors are limited between 0 and 0.3 p.u.

Meanwhile, voltage amplitudes of $P Q$ and $P V$ busbars are determined in $[0.9,1.1]$ p.u, including a set of 33-dimensional control variables.


Fig. 1.The internal distribution of IEEE 30


Fig. 2.The internal distribution of IEEE 57
A larger scale IEEE118-bus system will be applied to comprehensively evaluate the properties of IHCSA to deal with the MOOPF problem in a complex system.

Does Fig. 4 shows a single wireframing diagram of the IEEE118-bus system with 128 -dimensional vectors.


Fig. 3. The steps of the MOOPF problem with the IHCSA method


Fig. 4.The internal distribution of IEEE 118
TABLE II
OBJECT OF CASES

|  | $S_{\text {fcost }}$ | $S_{\text {emission }}$ | $S_{\text {Ploss }}$ | $S_{\text {fost-vp }}$ | $S_{V D}$ | Test System |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Case1 | $\checkmark$ |  | $\checkmark$ |  |  |  |
| Case2 | $\checkmark$ | $\checkmark$ |  |  |  |  |
| Case3 |  |  | $\checkmark$ | $\checkmark$ |  |  |
| Case4 | $\checkmark$ |  |  |  | $\checkmark$ | IEEE30 |
| Case5 | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |  |
| Case6 |  | $\checkmark$ | $\checkmark$ |  |  |  |
| Case7 | $\checkmark$ |  | $\checkmark$ |  |  |  |
| Case8 | $\checkmark$ | $\checkmark$ |  |  |  | IEEE57 |
| Case9 | $\checkmark$ |  | $\checkmark$ |  |  | IEEE118 |
| Case10 | $\checkmark$ | $\checkmark$ |  |  |  | IEEE118 |

The $P V$ bus voltage amplitude limit is the same as that of IEEE 57, and other detailed parameters of the IEEE118-bus system can be obtained in [28].

TABLE III
DETAILED PARAMETERS OF THE ALGORITHM

| Methods | Parameters | Case1-6 | Case7-8 | Case9-10 |
| :---: | :---: | :---: | :---: | :---: |
| IHCSA | Population Size NP | 100 | 100 | 100 |
|  | Maximum Iteration $K_{\text {max }}$ | 300 | 500 | 500 |
|  | Awareness Probability $A P_{\text {max }} / A P_{\text {min }}$ | 0.5/0.01 | 0.5/0.01 | 0.5/0.01 |
|  | fly length $f l$ | 0.8 | 0.8 | 0.8 |
|  | Zoom Scaling factor Fc | 0.6 | 0.6 | 0.6 |
|  | Crossed factor $C R$ | 0.8 | 0.8 | 0.8 |
| CSA | Population Size $N P$ | 100 | 100 | - |
|  | Maximum Iteration $K_{\text {max }}$ | 300 | 500 | - |
|  | Awareness Probability AP | 0.1 | 0.1 | - |
|  | fly length $f l$ | 2.0 | 3.5 | - |
| MOPSO | Population Size $N P$ | 100 | 100 | - |
|  | Maximum Iteration $K_{\text {max }}$ | 300 | 500 | - |
|  | Learning factor $\mathrm{cl} / \mathrm{c}_{2}$ | 2/2 | 2/2 | - |
|  | Inertia weight factor $\mathrm{w}_{\text {max }} / \mathrm{w}_{\text {min }}$ | 0.9/0.4 | 0.9/0.4 | - |
| NSGA-II | Population Size $N P$ | 100 | 100 | 100 |
|  | Maximum Iteration $K_{\text {max }}$ | 300 | 500 | 500 |
|  | Mutation index/percentage | 20/0.1 | 20/0.1 | 20/0.1 |
|  | Crossover index/percentage | 20/0.1 | 20/0.1 | 20/0.1 |



Fig. 5.PFs in different population sizes $\left(K_{\max }=300\right)$

## B. Algorithm Parameters

Considering the population size and the maximum number of iterations, a simulation experiment, which takes the cost of basic cost and power loss as objective functions, is carried out in the IEEE30-bus system to explore the influence of IHCSA. Fig. 5 reveals that IHCSA obtains the PFs in different population sizes under the same iteration number of 300 .

As can be seen from Fig. 5, IHCSA can obtain relatively evenly distributed PFs when the population size is $[30,50$, 80, 100, 120, 150]. It indicates that the IHCSA proposed in this paper can have a positive optimization effect on different scale of groups. That is, we can flexibly adjust the population size in practical application scenarios and use X for optimality search. Generally, when the population size is 100 and 150, the optimization effect of the IHCSA algorithm is more prominent. Considering the impact of running time, the crow population size is set as 100 in all experiments conducted in this paper. In addition, the performance of IHCSA under various $K_{\max }$ is studied.

In addition, Fig. 6 validates the PFs got by IHCSA in various $K_{\max }$ when the population scale is 100 .

Fig. 6 reveals that when $K_{\max }$ is set as 100, IHCSA obtains the worst PFs. Meanwhile, it gets the better PFs
when the maximum number of iterations is 200. Fig. 6 also verifies the uniform distribution of PFs obtained by iterating 300, 400, and 500 with similar efficiency. Therefore, we choose the maximum number of iterations $K_{\max }$ of 300 to reduce computational complexity.


Fig. 6.PFs in various iterations $(N P=100)$
C. IEEE 30

1) Casel

In Case1, the $S_{\text {fcost }}$ and $S_{\text {Ploss }}$, which have a competitive relationship, are optimized by proposed IHCSA, CSA, MOPSO, and NSGA-II approaches in the IEEE30-bus system.

Obviously, The PFs got by the above four methods have been depicted in Fig. 7. Moreover, the results denote that the particle filter performance obtained by IHCSA is significantly better than the ones obtained by MOPSO and NSGA-II. In addition, we are clearly informed that the performance of IHCSA is overwhelmingly superior to that of CSA, which shows that the improved method in this paper has a pronounced effect. It reveals that the proposed IHCSA has excellent potential to realize well-distributed PFs.

TABLE IV depicts the 24-dimensional control variables obtained by the four algorithms, and the BMS received
according to the equation (28). Among them, the BMS obtained by the IHCSA algorithm of $S_{\text {fcost }}$ and $S_{\text {Ploss }}$ are $833.4864 \$ / \mathrm{h}$ and 4.9817 MW . The ones gained by MOPSO, CSA, and NSGA-II methods, does not perform as well as the former. $C S$ depicts control solution.
For Case1, the comparison of BMS derived by different ways is depicted in TABLE V.

## 2) Case2

In Case2, the $S_{\text {fcost }}$ and $S_{\text {emission }}$, two important but weakly correlated quantities, need to be optimized concurrently.

Unsurprisingly, Fig. 8 represents PFs achieved by IHCSA, CSA, MOPSO, and NSGA-II methods.
TABLE VI reveals that the BMS obtained by IHCSA has advantages over the ones of the other algorithms. The BMS of the $S_{\text {fcost }}$ and $S_{\text {emission }}$ are $831.2109 \$ / \mathrm{h}$ and 0.2469 ton $/ \mathrm{h}$. Fig. 8 depicts the Pareto front derived by applying various methods.

TABLE IV

| CS | IHCSA | CSA | NSGA-II | MOPSO |
| :---: | :---: | :---: | :---: | :---: |
| $\mathrm{P}_{\text {Gen_2 }}(\mathrm{MW})$ | 53.7880 | 49.9306 | 56.9084 | 43.9687 |
| $\mathrm{P}_{\text {Gen_5 }}$ | 32.6786 | 33.6793 | 32.4266 | 31.3862 |
| $\mathrm{P}_{\text {Gen_8 }}$ | 35.0000 | 34.8733 | 33.9626 | 35.0000 |
| $\mathrm{P}_{\text {Gen_11 }}$ | 28.0230 | 26.4683 | 26.4354 | 30.0000 |
| $\mathrm{P}_{\text {Gen_13 }}$ | 20.7484 | 23.4341 | 21.4147 | 25.3434 |
| $\mathrm{V}_{\text {Gen_1 }}$ (p.u.) | 1.1000 | 1.0999 | 1.1000 | 1.0997 |
| $\mathrm{V}_{\text {Gen_2 }}$ | 1.0878 | 1.0895 | 1.0898 | 1.0921 |
| $\mathrm{V}_{\text {Gen_5 }}$ | 1.0617 | 1.0739 | 1.0652 | 1.0658 |
| $\mathrm{V}_{\text {Gen_8 }}$ | 1.0733 | 1.0774 | 1.0715 | 1.0764 |
| $\mathrm{V}_{\text {Gen_11 }}$ | 1.0999 | 1.0821 | 1.0273 | 1.0700 |
| $\mathrm{V}_{\text {Gen_13 }}$ | 1.0980 | 1.0933 | 1.0438 | 1.0960 |
| $\mathrm{T}_{11}$ (p.u.) | 0.9999 | 1.0937 | 1.0536 | 1.1000 |
| $\mathrm{T}_{12}$ | 0.9479 | 0.9049 | 0.9465 | 0.9000 |
| $\mathrm{T}_{15}$ | 0.9907 | 1.0247 | 1.0629 | 1.0432 |
| $\mathrm{T}_{36}$ | 0.9692 | 1.0153 | 1.0198 | 1.0109 |
| $\mathrm{Q}_{\mathrm{C} \_10}$ | 0.0334 | 0.0060 | 0.0170 | 0.0500 |
| $\mathrm{Q}_{\mathrm{C} \text { _12 }}$ | 0.0459 | 0.0480 | 0.0261 | 0.0208 |
| $\mathrm{Q}_{\mathrm{C} \text { _15 }}$ | 0.0337 | 0.0489 | 0.0016 | 0.0401 |
| $\mathrm{Q}_{\mathrm{C} \text { _17 }}$ | 0.0500 | 0.0456 | 0.0182 | 0.0475 |
| $\mathrm{Q}_{\mathrm{C} \text { _20 }}$ | 0.0419 | 0.0001 | 0.0431 | 0.0368 |
| $\mathrm{Q}_{\mathrm{C} \text { _21 }}$ | 0.0500 | 0.0415 | 0.0280 | 0.0404 |
| $\mathrm{Q}_{\mathrm{C} \text { _23 }}$ | 0.0381 | 0.0450 | 0.0302 | 0.0113 |
| $\mathrm{Q}_{\mathrm{C} \_24}$ | 0.0445 | 0.0484 | 0.0451 | 0.0170 |
| $\mathrm{Q}_{\mathrm{C} \text { _29 }}$ | 0.0235 | 0.0365 | 0.0148 | 0.0402 |
| $S_{\text {Ploss }}$ (MW) | 4.9817 | 5.0586 | 5.2265 | 5.1268 |
| $S_{\text {fcost }}(\$ / \mathrm{h})$ | 833.4864 | 834.2233 | 833.6061 | 834.5184 |



Fig. 7.PFs of Case 1

The BMS of Case 2 derived by various ways denoted by other academicians in recent years are depicted in TABLE VII.

From the details of TABLE VII, The BMS derived by IHCSA is superior to the ones obtained by NSGA-III, ESDE, and AGSO and has the same competitive advantage as the BMS derived by DE-PFA, MOEA/D, MODFA, and MGBICA. In conclusion, compared with other algorithms proposed by other scholars, the proposed algorithm has better competitive advantages.

TABLE V
VARIOUS BMS FOR CASE1

| VARIOUS BMS FOR CASE1 |  |  |
| :---: | :---: | :---: |
| Comparison | $S_{\text {fcost }}(\$ / \mathrm{h})$ | $S_{\text {Ploss }}(/ \mathrm{MW})$ |
| IHCSA | $\mathbf{8 3 3 . 4 8 6 4}$ | $\mathbf{4 . 9 8 1 7}$ |
| CSA | 834.2233 | 5.0586 |
| NSGA-II | 833.6061 | 5.2265 |
| MOPSO | 834.5184 | 5.1268 |
| NSGA-III[27] | 836.8076 | 5.1775 |
| MODFA[27] | 833.9365 | 4.9561 |

TABLE VI
DETAILS OF BMS FOR CASE2

| CS | IHCSA | CSA | NSGA-II | MOPSO |
| :---: | :---: | :---: | :---: | :---: |
| $\mathrm{P}_{\text {Gen_2 }}(\mathrm{MW})$ | 57.9900 | 58.9863 | 58.9102 | 59.8005 |
| $\mathrm{P}_{\text {Gen_5 }}$ | 25.6644 | 26.5294 | 28.2860 | 25.0199 |
| $\mathrm{P}_{\text {Gen_8 }}$ | 35.0000 | 34.9108 | 34.9837 | 33.0113 |
| $\mathrm{P}_{\text {Gen_11 }}$ | 27.0888 | 27.1162 | 25.4120 | 23.5310 |
| $\mathrm{P}_{\text {Gen_13 }}$ | 26.2415 | 24.7357 | 24.4445 | 29.5362 |
| $\mathrm{V}_{\text {Gen_1 }}(\mathrm{p} . \mathrm{u}$. | 1.1000 | 1.0967 | 1.0589 | 1.1000 |
| $\mathrm{V}_{\text {Gen_2 }}$ | 1.0876 | 1.0870 | 1.0467 | 1.0916 |
| $\mathrm{V}_{\text {Gen_5 }}$ | 1.0666 | 1.0525 | 1.0117 | 1.0486 |
| $\mathrm{V}_{\text {Gen_8 }}$ | 1.0676 | 1.0635 | 1.0249 | 1.0790 |
| $\mathrm{V}_{\text {Gen_11 }}$ | 1.0973 | 0.9844 | 1.0810 | 1.0896 |
| $\mathrm{V}_{\text {Gen_13 }}$ | 1.0766 | 1.0590 | 1.0567 | 1.0807 |
| $\mathrm{T}_{11}$ (p.u.) | 1.0410 | 1.0662 | 0.9083 | 0.9978 |
| $\mathrm{T}_{12}$ | 0.9447 | 0.9500 | 1.0466 | 0.9875 |
| $\mathrm{T}_{15}$ | 1.0090 | 1.0939 | 0.9972 | 1.1000 |
| $\mathrm{T}_{36}$ | 0.9888 | 1.0371 | 0.9757 | 1.0280 |
| $\mathrm{Q}_{\mathrm{C} \text { _10 }}$ | 0.0368 | 0.0414 | 0.0347 | 0.0240 |
| $\mathrm{Q}_{\mathrm{C} \text { _12 }}$ | 0.0500 | 0.0016 | 0.0471 | 0.0500 |
| $\mathrm{Q}_{\mathrm{C} 15}$ | 0.0438 | 0.0115 | 0.0018 | 0.0320 |
| Q C _17 | 0.0358 | 0.0297 | 0.0114 | 0.0500 |
| $\mathrm{Q}_{\mathrm{C} \_20}$ | 0.0500 | 0.0180 | 0.0056 | 0.0294 |
| $\mathrm{Q}_{\mathrm{C} \text { 21 }}$ | 0.0416 | 0.0001 | 0.0408 | 0.0490 |
| $\mathrm{Q}_{\mathrm{C} \text { _23 }}$ | 0.0221 | 0.0498 | 0.0478 | 0.0066 |
| $\mathrm{Q}_{\mathrm{C} \text { 24 }}$ | 0.0500 | 0.0179 | 0.0356 | 0.0300 |
| $\mathrm{Q}_{\mathrm{C} \_29}$ | 0.0308 | 0.0498 | 0.0334 | 0.0349 |
| $S_{\text {emission }}$ (MW) | 0.2469 | 0.2472 | 0.2478 | 0.2492 |
| $S_{\text {fcost }}(\$ / \mathrm{h})$ | 831.2109 | 831.9036 | 832.3313 | 831.3669 |

TABLE VII
VARIOUS BMS FOR CASE2

| Comparison | $S_{\text {fcost }}(/ \$)$ | $S_{\text {emission }}($ ton $/ \mathrm{h})$ |
| :---: | :---: | :---: |
| IHCSA | $\mathbf{8 3 1 . 2 1 0 9}$ | $\mathbf{0 . 2 4 6 4}$ |
| CSA | 831.9036 | 0.2472 |
| NSGA-II | 832.3313 | 0.2478 |
| MOPSO | 831.3669 | 0.2492 |
| NSGA-III[27] | 832.5323 | 0.2483 |
| DE-PFA[28] | 833.5200 | 0.2332 |

## 3) Case 3

In Case3, IHCSA and the other three algorithms are applied to optimize $S_{\text {Ploss }}$ and $S_{\text {fcost_vp }}$ simultaneously. As shown in TABLE VIII, the BMS obtained by the IHCSA algorithm has advantages over the other three algorithms, including $S_{\text {fcost_vp }}$ of $864.7519 \$ / \mathrm{h}$ and $S_{\text {Ploss }}$ of 5.5995 MW . Fig. 9 reveals the Pareto front of POS obtained by the

IHCSA algorithm is more prominent, indicating that the effect of the proposed method is remarkable.
TABLE IX denotes that compared with the algorithms proposed by other scholars, the BMS obtained by IHCSA has more advantages.


Fig. 8.PFs of Case2
TABLE VIII

| CS | IHCSA | CSA | NSGA-II | MOPSO |
| :---: | :---: | :---: | :---: | :---: |
| $\mathrm{P}_{\text {Gen_2 }}(\mathrm{MW})$ | 44.5546 | 46.4769 | 44.7199 | 40.0518 |
| $\mathrm{P}_{\text {Gen_5 }}$ | 30.7240 | 33.9651 | 29.7495 | 30.0146 |
| $\mathrm{P}_{\text {Gen_8 }}$ | 34.8646 | 34.8515 | 34.9995 | 35.0000 |
| $\mathrm{P}_{\text {Gen_11 }}$ | 28.0515 | 19.2982 | 27.0462 | 30.0000 |
| $\mathrm{P}_{\text {Gen_13 }}$ | 15.8929 | 19.7758 | 18.7778 | 17.3900 |
| $\mathrm{V}_{\text {Gen_l }}(\mathrm{p} . \mathrm{u}$. | 1.1000 | 1.0994 | 1.0962 | 1.1000 |
| $\mathrm{V}_{\text {Gen_2 }}$ | 1.0862 | 1.0886 | 1.0821 | 1.0850 |
| $\mathrm{V}_{\text {Gen_5 }}$ | 1.0634 | 1.0676 | 1.0552 | 1.0591 |
| $\mathrm{V}_{\text {Gen_8 }}$ | 1.0706 | 1.0712 | 1.0679 | 1.0677 |
| $\mathrm{V}_{\text {Gen_11 }}$ | 1.1000 | 1.0666 | 1.0717 | 1.0925 |
| $\mathrm{V}_{\text {Gen_13 }}$ | 1.0997 | 1.0839 | 1.0973 | 1.0845 |
| $\mathrm{T}_{11}$ (p.u.) | 1.0149 | 1.0287 | 0.9821 | 1.0636 |
| $\mathrm{T}_{12}$ | 0.9344 | 0.9559 | 0.9503 | 0.9000 |
| $\mathrm{T}_{15}$ | 0.9896 | 1.0013 | 0.9953 | 1.0032 |
| $\mathrm{T}_{36}$ | 0.9685 | 0.9912 | 0.9848 | 0.9825 |
| $\mathrm{Q}_{\mathrm{C} \text { _10 }}$ | 0.0481 | 0.0092 | 0.0500 | 0.0192 |
| $\mathrm{Q}_{\mathrm{C} \text { _12 }}$ | 0.0500 | 0.0158 | 0.0372 | 0.0136 |
| $\mathrm{Q}_{\mathrm{C} \text { _1 }}$ | 0.0345 | 0.0020 | 0.0260 | 0.0373 |
| $\mathrm{Q}_{\mathrm{C} \text { _17 }}$ | 0.0500 | 0.0105 | 0.0167 | 0.0284 |
| $\mathrm{Q}_{\mathrm{C} \text { _20 }}$ | 0.0348 | 0.0456 | 0.0432 | 0.0500 |
| $\mathrm{Q}_{\mathrm{C} \text { 21 }}$ | 0.0500 | 0.0449 | 0.0380 | 0.0500 |
| $\mathrm{Q}_{\mathrm{C} \text { _23 }}$ | 0.0390 | 0.0281 | 0.0159 | 0.0430 |
| $\mathrm{Q}_{\mathrm{C} \text { _24 }}$ | 0.0500 | 0.0290 | 0.0466 | 0.0500 |
| Q C _29 | 0.0290 | 0.0347 | 0.0242 | 0.0337 |
| $S_{\text {Ploss }}(\mathrm{MW})$ | 5.5995 | 5.7337 | 5.6830 | 5.6490 |
| $S_{\text {fcost-vp }}(\$ / \mathrm{h})$ | 864.7519 | 865.7643 | 866.0764 | 867.3759 |

## 4) Case4

In Case4, two objectives are considered and optimized concurrently by various methods, including basic fuel cost and voltage deviation. TABLE $X$ indicates that the BMS obtained by the IHCSA algorithm includes a voltage deviation of 0.4366 and basic fuel cost of $799.6643 \$ / \mathrm{h}$.

As can be seen from Fig. 10, the Pareto frontier of IHCSA has more advantages than CSA and NSGA-II. The Pareto frontier of the MOPSO algorithm is not ideal, so no comparison is made.


Fig. 9.PFs of Case3

TABLE IX
VARIOUS BMS FOR CASE3

|  | CARI |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Comparison | $S_{\text {fcost_vp }}(\$ / \mathrm{h})$ | $S_{\text {Ploss }}(/ \mathrm{MW})$ |  |  |
| IHCSA | $\mathbf{8 6 4 . 7 5 1 9}$ | $\mathbf{5 . 5 9 9 5}$ |  |  |
| CSA | 865.7643 | 5.7337 |  |  |
| NSGA-II | 866.0764 | 5.6830 |  |  |
| MOPSO | 867.3759 | 5.6490 |  |  |
| MHFPA[40] | 867.8159 | 5.6303 |  |  |
| NHBA[28] | 868.9526 | 5.6761 |  |  |

TABLE X
DETAILS OF BMS FOR CASE4

| CS | IHCSA | CSA | NSGA-II |
| :---: | :---: | :---: | :---: |
| $\mathrm{P}_{\text {Gen_2 }}(\mathrm{MW})$ | 49.6677 | 49.6029 | 48.9956 |
| $\mathrm{P}_{\text {Gen_5 }}$ | 21.1507 | 21.8197 | 21.2636 |
| $\mathrm{P}_{\text {Gen_8 }}$ | 21.3810 | 20.4622 | 21.3171 |
| $\mathrm{P}_{\text {Gen_11 }}$ | 11.7276 | 13.4931 | 10.6560 |
| $\mathrm{P}_{\text {Gen_13 }}$ | 12.0223 | 12.2405 | 12.0521 |
| $\mathrm{V}_{\text {Gen_1 }}$ (p.u.) | 1.1000 | 1.0542 | 1.0995 |
| $\mathrm{V}_{\text {Gen_2 }}$ | 1.0869 | 1.0342 | 1.0837 |
| $\mathrm{V}_{\text {Gen_5 }}$ | 1.0529 | 0.9987 | 1.0532 |
| $\mathrm{V}_{\text {Gen_8 }}$ | 1.0624 | 0.9992 | 1.0618 |
| $\mathrm{V}_{\text {Gen_11 }}$ | 1.0335 | 1.0144 | 1.0454 |
| $\mathrm{V}_{\text {Gen_13 }}$ | 1.0338 | 1.0309 | 1.0494 |
| $\mathrm{T}_{11}$ (p.u.) | 1.0485 | 0.9365 | 1.0159 |
| $\mathrm{T}_{12}$ | 1.0331 | 0.9597 | 1.0765 |
| $\mathrm{T}_{15}$ | 1.0713 | 0.9717 | 1.0799 |
| $\mathrm{T}_{36}$ | 1.0094 | 0.9440 | 1.0273 |
| $\mathrm{Q}_{\mathrm{C} \_10}$ | 0.0414 | 0.0230 | 0.0495 |
| $\mathrm{Q}_{\mathrm{C} \text { _12 }}$ | 0.0000 | 0.0361 | 0.0358 |
| $\mathrm{Q}_{\mathrm{C} \text { _15 }}$ | 0.0461 | 0.0142 | 0.0095 |
| $\mathrm{Q}_{\mathrm{C} \text { _17 }}$ | 0.0292 | 0.0294 | 0.0414 |
| $\mathrm{Q}_{\mathrm{C} \text { _20 }}$ | 0.0500 | 0.0131 | 0.0220 |
| $\mathrm{Q}_{\mathrm{C} \text { _21 }}$ | 0.0358 | 0.0249 | 0.0279 |
| $\mathrm{Q}_{\mathrm{C} \text { _23 }}$ | 0.0287 | 0.0233 | 0.0244 |
| $\mathrm{Q}_{\mathrm{C} \text { _24 }}$ | 0.0500 | 0.0296 | 0.0500 |
| $\mathrm{Q}_{\mathrm{C} \_29}$ | 0.0182 | 0.0109 | 0.0258 |
| $S_{V D}$ | 0.4366 | 0.2132 | 0.4681 |
| $S_{\text {fcost }}(\$ / \mathrm{h})$ | 799.6643 | 803.2034 | 799.6652 |

## 5) Case5

In Case5, the $S_{\text {fcost }}, S_{\text {emission }}$, and $S_{\text {Ploss }}$ are optimized concurrently. TABLE XI reveals that the BMS obtained by IHCSA has more advantages, including $S_{\text {emission }}$ of 0.2177 ton $/ \mathrm{h}, S_{\text {Ploss }}$ of 4.0638 MW , and $S_{\text {fcost }}$ of $876.2110 \$ / \mathrm{h}$.

For Case5, the comparison of the BMS obtained by different algorithms is denoted in TABLE XIII.

Fig. 11 shows that Pareto front of IHCSA is nearer actual Pareto front than CSA, NSGA-II, and MOPSO.


Fig. 10. PFs of Case4

TABLE XI
DETAILS OF BMS FOR CASE5

| CS | IHCSA | CSA | NSGA-II | MOPSO |
| :---: | :---: | :---: | :---: | :---: |
| $\mathrm{P}_{\text {Gen } 22}(\mathrm{MW})$ | 59.2651 | 66.5689 | 62.5712 | 80.000 |
| $\mathrm{P}_{\text {Gen_5 }}$ | 37.4872 | 38.2036 | 41.5270 | 33.8435 |
| $\mathrm{P}_{\text {Gen_8 }}$ | 35.0000 | 34.0128 | 34.7084 | 35.0000 |
| $\mathrm{P}_{\text {Gen_11 }}$ | 30.0000 | 28.7128 | 28.3620 | 27.3982 |
| $\mathrm{P}_{\text {Gen_13 }}$ | 35.6421 | 32.8182 | 32.1899 | 32.1505 |
| $\mathrm{V}_{\text {Gen_1 }}$ (p.u.) | 1.1000 | 1.0811 | 1.0508 | 1.1000 |
| $\mathrm{V}_{\text {Gen_2 }}$ | 1.0871 | 1.07017 | 1.0443 | 1.1000 |
| $\mathrm{V}_{\text {Gen_5 }}$ | 1.0641 | 1.0412 | 1.0209 | 1.0795 |
| $\mathrm{V}_{\text {Gen_8 }}$ | 1.0739 | 1.0380 | 1.0260 | 1.0787 |
| $\mathrm{V}_{\text {Gen_11 }}$ | 1.0777 | 1.0686 | 1.0614 | 1.1000 |
| $\mathrm{V}_{\text {Gen_13 }}$ | 1.0656 | 1.0851 | 1.0682 | 1.0895 |
| $\mathrm{T}_{11}$ (p.u.) | 1.0072 | 0.9135 | 0.9409 | 0.9801 |
| $\mathrm{T}_{12}$ | 1.0287 | 0.9563 | 1.0053 | 1.0670 |
| $\mathrm{T}_{15}$ | 1.0489 | 0.9491 | 1.0269 | 0.9774 |
| $\mathrm{T}_{36}$ | 1.0215 | 0.9463 | 0.9666 | 0.9599 |
| $\mathrm{Q}_{\mathrm{C} \text { _10 }}$ | 0.0149 | 0.0139 | 0.0178 | 0.0500 |
| $\mathrm{QC}_{\text {c } 12}$ | 0.0283 | 0.0041 | 0.0287 | 0.0004 |
| $\mathrm{Q}_{\mathrm{C} \text { _15 }}$ | 0.0454 | 0.0427 | 0.0325 | 0.0158 |
| $\mathrm{Q}_{\mathrm{C} \text { _17 }}$ | 0.0444 | 0.0488 | 0.0144 | 0.0323 |
| $\mathrm{Q}_{\mathrm{C} \text { _20 }}$ | 0.0500 | 0.0472 | 0.0215 | 0.0454 |
| Q C _21 | 0.0127 | 0.0161 | 0.0471 | 0.0447 |
| $\mathrm{Q}_{\mathrm{C} \text { _23 }}$ | 0.0327 | 0.0125 | 0.0014 | 0.0321 |
| Q C _24 | 0.0274 | 0.0136 | 0.0367 | 0.0406 |
| QC_29 | 0.0255 | 0.0300 | 0.0420 | 0.0283 |
| $S_{\text {emission }}(\mathrm{ton} / \mathrm{h})$ | 0.2177 | 0.2184 | 0.2177 | 0.2203 |
| $S_{\text {Ploss }}(\mathrm{MW})$ | 4.0638 | 4.3548 | 4.2449 | 4.1235 |
| $S_{\text {fcost }}(\$ / \mathrm{h})$ | 876.2110 | 879.3365 | 883.6450 | 886.3948 |

## 6) Case6

In Case6, the power loss and emission are chosen to be optimized simultaneously. The BMS obtained by four algorithms, including IHCSA, CSA, NSGA-II, and MOPSO, are shown in TABLE XII.
It is apparent from the table the BMS gained by IHCSA of the emission and the active power loss is 0.2053 ton $/ \mathrm{h}$ and 2.8929 MW. The Pareto front of their POS is indicated in Fig. 12. It is evident that the Pareto front of the IHCSA algorithm has outstanding advantages.

TABLE XIV indicates that compared to other researches, the BMS obtained by IHCSA has strong competitiveness.


Fig. 11. PFs of Case5


Fig. 12. PFs of Case6
TABLE XII
DETAILS OF BMS FOR CASE6

| CS | IHCSA | CSA | NSGA-II | MOPSO |
| :---: | :---: | :---: | :---: | :---: |
| $\mathrm{P}_{\text {Gen } 22}(\mathrm{MW})$ | 73.5921 | 73.4866 | 73.7064 | 73.1661 |
| $\mathrm{P}_{\text {Gen_5 }}$ | 50.0000 | 49.9996 | 49.9992 | 49.9271 |
| $\mathrm{P}_{\text {Gen_8 }}$ | 34.9999 | 34.9917 | 34.9999 | 34.9268 |
| $\mathrm{P}_{\text {Gen_11 }}$ | 30.0000 | 29.9992 | 29.9987 | 29.9741 |
| $\mathrm{P}_{\text {Gen_13 }}$ | 40.0000 | 39.9979 | 39.9992 | 39.9879 |
| $\mathrm{V}_{\text {Gen_1 }}$ (p.u.) | 1.1000 | 1.1000 | 1.0759 | 1.0999 |
| $\mathrm{V}_{\text {Gen_2 }}$ | 1.0964 | 1.1000 | 1.0712 | 1.0984 |
| $\mathrm{V}_{\text {Gen_5 }}$ | 1.07841 | 1.0863 | 1.0530 | 1.0801 |
| $\mathrm{V}_{\text {Gen_8 }}$ | 1.0856 | 1.0986 | 1.0589 | 1.0854 |
| $\mathrm{V}_{\text {Gen_11 }}$ | 1.1000 | 1.0817 | 1.0980 | 1.1000 |
| $\mathrm{V}_{\text {Gen_13 }}$ | 1.1000 | 1.1000 | 1.0998 | 1.0940 |
| $\mathrm{T}_{11}$ (p.u.) | 1.0208 | 0.9614 | 1.0115 | 1.0144 |
| $\mathrm{T}_{12}$ | 0.9287 | 1.0772 | 0.9000 | 0.9860 |
| $\mathrm{T}_{15}$ | 0.9867 | 1.0055 | 0.9646 | 0.9855 |
| $\mathrm{T}_{36}$ | 0.9706 | 1.0186 | 0.9523 | 0.9999 |
| $\mathrm{Q}_{\mathrm{C} \_10}$ | 0.0211 | 0.0500 | 0.0479 | 0.0480 |
| $\mathrm{Q}_{\mathrm{C} \text { _12 }}$ | 0.0500 | 0.0005 | 0.0479 | 0.0000 |
| $\mathrm{Q}_{\mathrm{C} \text { _15 }}$ | 0.0401 | 0.0000 | 0.0500 | 0.0455 |
| $\mathrm{Q}_{\mathrm{C} \text { _17 }}$ | 0.0500 | 0.0000 | 0.0469 | 0.0500 |
| $\mathrm{Q}_{\mathrm{C} \text { _20 }}$ | 0.0441 | 0.0375 | 0.0288 | 0.0306 |
| $\mathrm{Q}_{\mathrm{C} \text { 21 }}$ | 0.0500 | 0.0419 | 0.0479 | 0.0500 |
| $\mathrm{Q}_{\mathrm{C} \text { _23 }}$ | 0.0292 | 0.0500 | 0.0317 | 0.0142 |
| $\mathrm{Q}_{\mathrm{C} \text { _24 }}$ | 0.0500 | 0.0462 | 0.0483 | 0.0419 |
| QC_29 | 0.0203 | 0.0469 | 0.0229 | 0.0398 |
| $S_{\text {emission }}(\mathrm{ton} / \mathrm{h})$ | 0.2053 | 0.2053 | 0.2053 | 0.2053 |
| $S_{\text {Ploss }}(\mathrm{MW})$ | 2.8929 | 3.0333 | 2.9872 | 2.9508 |

TABLE XIII
VARIOUS BMS FOR CASE5

| Comparison | $S_{\text {emission }}$ <br> (ton/h) | $\left.S_{\text {Ploss }} / \mathrm{MW}\right)$ | $S_{\text {fcost }}(\$ / \mathrm{h})$ |
| :---: | :---: | :---: | :---: |
| IHCSA | $\mathbf{0 . 2 1 7 7}$ | $\mathbf{4 . 0 6 3 8}$ | $\mathbf{8 7 6 . 2 1 1 0}$ |
| CSA | 0.2184 | 4.3548 | 879.3365 |
| NSGA-II | 0.2177 | 4.2449 | 883.6450 |
| MOPSO | 0.2203 | 4.1235 | 886.3948 |
| MHFPA[40] | 0.2167 | 3.9070 | 879.4391 |

TABLE XIV
VARIOUS BMS FOR CASE6

| Comparison | $S_{\text {emission }}($ ton $/ \mathrm{h})$ | $S_{\text {Ploss }}$ (/MW) |
| :---: | :---: | :---: |
| IHCSA | $\mathbf{0 . 2 0 5 3}$ | $\mathbf{2 . 8 9 2 9}$ |
| CSA | 0.2053 | 3.0333 |
| NSGA-II | 0.2053 | 2.9872 |
| MOPSO | 0.2053 | 2.9508 |
| MODFA[27] | 0.2054 | 2.8830 |

TABLE XV
DETAILS OF BMS FOR CASE7

| CS | IHCSA | CSA | NSGA-II |
| :---: | :---: | :---: | :---: |
| $\mathrm{P}_{\text {Gen_2 } 2}(\mathrm{MW})$ | 72.9442 | 99.9283 | 71.3663 |
| $\mathrm{P}_{\text {Gen_3 }}$ | 57.4972 | 66.5498 | 55.8950 |
| $\mathrm{P}_{\text {Gen_6 }}$ | 90.7924 | 76.8989 | 85.5446 |
| $\mathrm{P}_{\text {Gen_8 }}$ | 378.3653 | 372.3670 | 392.4783 |
| $\mathrm{P}_{\text {Gen_9 }}$ | 100.0000 | 100.0000 | 100.0000 |
| $\mathrm{P}_{\text {Gen_12 }}$ | 410.0000 | 410.0000 | 408.5869 |
| $\mathrm{V}_{\text {Gen_1 }}(\mathrm{p} . \mathrm{u}$. | 1.0568 | 1.0872 | 0.9863 |
| $\mathrm{V}_{\text {Gen_2 }}$ | 1.0533 | 1.0867 | 0.9834 |
| $\mathrm{V}_{\text {Gen_3 }}$ | 1.0467 | 1.0833 | 0.9815 |
| $\mathrm{V}_{\text {Gen_6 }}$ | 1.0513 | 1.0810 | 1.0007 |
| $\mathrm{V}_{\text {Gen_8 }}$ | 1.0545 | 1.0818 | 1.0089 |
| $\mathrm{V}_{\text {Gen_9 }}$ | 1.0473 | 1.0779 | 0.9983 |
| $\mathrm{V}_{\text {Gen_12 }}$ | 1.0453 | 1.0751 | 0.9844 |
| $\mathrm{T}_{19}$ (p.u.) | 1.0130 | 0.9160 | 0.9776 |
| $\mathrm{T}_{20}$ | 0.9117 | 1.0354 | 1.0287 |
| $\mathrm{T}_{31}$ | 0.9796 | 1.0996 | 1.0084 |
| $\mathrm{T}_{35}$ | 0.9988 | 1.0177 | 1.0080 |
| T36 | 1.0123 | 1.0769 | 1.0162 |
| $\mathrm{T}_{37}$ | 1.0362 | 1.0291 | 0.9463 |
| $\mathrm{T}_{41}$ | 0.9952 | 1.0232 | 0.9108 |
| $\mathrm{T}_{46}$ | 0.9587 | 0.9729 | 0.9464 |
| $\mathrm{T}_{54}$ | 0.9012 | 0.9659 | 0.9023 |
| $\mathrm{T}_{58}$ | 0.9611 | 0.9995 | 0.9244 |
| $\mathrm{T}_{59}$ | 0.9570 | 1.0184 | 0.9262 |
| $\mathrm{T}_{65}$ | 0.9944 | 1.0030 | 0.9361 |
| $\mathrm{T}_{66}$ | 0.9311 | 0.9711 | 0.9076 |
| $\mathrm{T}_{71}$ | 0.9476 | 0.9877 | 0.9574 |
| $\mathrm{T}_{73}$ | 0.9727 | 0.9576 | 1.0041 |
| $\mathrm{T}_{76}$ | 0.9514 | 1.0365 | 0.9237 |
| $\mathrm{T}_{80}$ | 1.0144 | 1.0207 | 0.9360 |
| $\mathrm{Q}_{\mathrm{C} \_18}$ (p.u.) | 0.1002 | 0.0966 | 0.1895 |
| QC_25 | 0.1522 | 0.1446 | 0.2089 |
| Q C _53 | 0.1372 | 0.1870 | 0.1488 |
| $S_{\text {Ploss }}$ (MW) | 11.3468 | 11.4242 | 12.7539 |
| $S_{\text {fcost }}(\$ / \mathrm{h})$ | 41989.0500 | 42096.1600 | 41961.0000 |

## D. IEEE 57

## 1) $C a s e 7$

In Case7, the $S_{\text {fcost }}$ and $S_{\text {Ploss }}$ are still treated as two weakly correlated targets for optimization, however, the platform for testing is changed to the IEEE57-bus system.
In this case, since the POS of the MOPSO algorithm cannot obtain an effective Pareto front, its analysis is not carried out. The BMS of IHCSA, CSA, and NSGA-II are depicted in TABLE XV.
As shown in the table, the one gained by proposed approach includes $S_{\text {Ploss }}$ of 11.3468 MW and $S_{\text {foss }}$ of 41989.0500 \$/h.

It is apparent from Fig. 13 that the Pareto front of the POS obtained by IHCSA has a greater tendency to be appreciated by managers. There is no doubt that compared with the other two algorithms, IHCSA has more advantages.


Fig. 13. PFs of Case7
TABLE XVI

| VARIOUS BMS FOR CASE7 |  |  |
| :---: | :---: | :---: |
| Algorithms | $S_{\text {fcost }}(\$ / \mathrm{h})$ | $S_{\text {Ploss }}(/ \mathrm{MW})$ |
| IHCSA | $\mathbf{4 1 9 8 9 . 0 5 0 0}$ | $\mathbf{1 1 . 3 4 6 8}$ |
| CSA | 42096.1600 | 11.4242 |
| NSGA-II | 41961.0000 | 12.7539 |
| ESDE-MC[24] | 41998.3588 | 11.8415 |



Fig. 14. PFs of Case8
TABLE XVII
VARIOUS BMS FOR CASE8

| Comparison | $S_{\text {fcost }}(\$ / \mathrm{h})$ | $S_{\text {emission }}($ ton $/ \mathrm{h})$ |
| :---: | :---: | :---: |
| IHCSA | $\mathbf{4 2 9 2 3 . 5 9 0 0}$ | $\mathbf{1 . 2 9 8 9}$ |
| CSA | 43125.2700 | 1.3194 |
| NSGA-II | 43007.9400 | 1.3518 |
| MOPSO | 43056.2700 | 1.3100 |
| MODFA[27] | 43174.5700 | 1.2679 |
| NSGA-III[27] | 43398.7500 | 1.2530 |

TABLE XVIII

| VARIOUS BMS FOR CASE9 |  |  |
| :---: | :---: | :---: |
| Algorithms | $S_{\text {fcost }}(\$ / \mathrm{h})$ | $S_{\text {Ploss }}(/ \mathrm{MW})$ |
| IHCSA | $\mathbf{5 8 5 1 3 . 8 9 0 0}$ | $\mathbf{5 4 . 3 8 0 3}$ |
| NSGA-II | 59366.9100 | 56.8467 |
| HFBA-COFS[28] | 59624.0613 | 61.0362 |

## 2) Case 8

In Case8, the $S_{\text {fcost }}$ and $S_{\text {emission }}$ are synchronously optimized by four algorithms to reflect the distinctions between the different methods. As shown in Fig. 14, compared with CSA, NSGA-II and MOPSO, the Pareto front gained by IHCSA is nearer to the real Pareto front and has more advantages. The BMS and corresponding variables obtained are depicted in TABLE XIX, including emission of $1.2989 \mathrm{ton} / \mathrm{h}$ and fuel cost of $42923.5900 \$ / \mathrm{h}$.

TABLE XIX
DETAILS OF BMS FOR CASE8

| CS | IHCSA | CSA | NSGA-II | MOPSO |
| :---: | :---: | :---: | :---: | :---: |
| $\mathrm{P}_{\text {Gen_2 }}(\mathrm{MW})$ | 100.0000 | 93.1424 | 99.8112 | 100.0000 |
| $\mathrm{P}_{\text {Gen_3 }}$ | 81.9845 | 87.7182 | 76.7071 | 100.9952 |
| $\mathrm{P}_{\text {Gen_6 }}$ | 100.0000 | 98.8348 | 100.0000 | 97.7089 |
| $\mathrm{P}_{\text {Gen_8 }}$ | 334.9970 | 342.1080 | 350.3993 | 360.8372 |
| $\mathrm{P}_{\text {Gen_9 }}$ | 100.0000 | 92.0777 | 99.9511 | 100.0000 |
| $\mathrm{P}_{\text {Gen_12 }}$ | 332.6469 | 329.4928 | 332.6281 | 313.0755 |
| $\mathrm{V}_{\text {Gen_1 }}$ (p.u.) | 1.0481 | 1.0985 | 0.9421 | 1.1000 |
| $\mathrm{V}_{\text {Gen_2 }}$ | 1.0460 | 1.0965 | 0.9376 | 1.1000 |
| $\mathrm{V}_{\text {Gen_3 }}$ | 1.0407 | 1.0907 | 0.9566 | 1.1000 |
| $\mathrm{V}_{\text {Gen_6 }}$ | 1.0428 | 1.0863 | 0.9965 | 1.1000 |
| $\mathrm{V}_{\text {Gen_8 }}$ | 1.0512 | 1.0827 | 1.0301 | 1.1000 |
| $\mathrm{V}_{\text {Gen_9 }}$ | 1.0408 | 1.0694 | 1.0119 | 1.1000 |
| $\mathrm{V}_{\text {Gen_12 }}$ | 1.0274 | 1.0679 | 1.0079 | 1.1000 |
| $\mathrm{T}_{19}$ (p.u.) | 1.0173 | 0.9458 | 1.0054 | 0.9197 |
| $\mathrm{T}_{20}$ | 0.9349 | 1.0988 | 1.0120 | 1.0745 |
| $\mathrm{T}_{31}$ | 1.0043 | 1.0883 | 0.9077 | 1.1000 |
| T35 | 0.9982 | 0.9974 | 0.9400 | 1.1000 |
| $\mathrm{T}_{36}$ | 0.9640 | 0.9214 | 1.0998 | 1.0426 |
| T37 | 1.0320 | 1.0884 | 1.0304 | 1.0781 |
| T 41 | 0.9837 | 0.9846 | 0.9776 | 1.0346 |
| $\mathrm{T}_{46}$ | 0.9326 | 0.9007 | 1.0244 | 0.9352 |
| $\mathrm{T}_{54}$ | 0.9251 | 0.9059 | 0.9074 | 0.9309 |
| $\mathrm{T}_{58}$ | 0.9590 | 0.9757 | 0.9011 | 1.0242 |
| $\mathrm{T}_{59}$ | 0.9472 | 1.0068 | 0.9146 | 1.0046 |
| $\mathrm{T}_{65}$ | 0.9559 | 1.0316 | 0.9839 | 1.0482 |
| $\mathrm{T}_{66}$ | 0.9287 | 0.9402 | 0.9999 | 0.9860 |
| $\mathrm{T}_{71}$ | 0.9529 | 1.0865 | 1.0081 | 0.9888 |
| $\mathrm{T}_{73}$ | 1.0137 | 0.9013 | 1.0093 | 0.9861 |
| $\mathrm{T}_{76}$ | 0.9670 | 1.0148 | 0.9567 | 0.9874 |
| $\mathrm{T}_{80}$ | 0.9936 | 1.0337 | 0.9812 | 1.0950 |
| $\mathrm{Q}_{\mathrm{C} \_18}$ (p.u.) | 0.0575 | 0.2035 | 0.1329 | 0.0135 |
| $\mathrm{Q}_{\mathrm{C} \text { 25 }}$ | 0.1290 | 0.0025 | 0.2648 | 0.1894 |
| $\mathrm{Q}_{\mathrm{C} \text { _53 }}$ | 0.1266 | 0.0240 | 0.1667 | 0.2987 |
| $S_{\text {emission }}(\mathrm{ton} / \mathrm{h})$ | 1.2989 | 1.3194 | 1.3518 | 1.3100 |
| $S_{\text {fcost }}(\$ / \mathrm{h})$ | 42923.5900 | 43125.2700 | 43007.9400 | 43056.2700 |

TABLE XVII reveals that compared with other scholars' methods, the BMS obtained by IHCSA has a more significant advantage in basic fuel cost. Meanwhile, IHCSA can also achieve good results in optimizing emissions.

## E. IEEE 118

Due to the uniqueness and complex structure of the IEEE 118-bus system, few scholars have studied the adaptability of their methods above. Because the work is quite difficult. 1) Case9

In Case9, the $S_{\text {fcost }}$ and $S_{\text {Ploss }}$ will be calculated in the IEEE118-bus system which is more challenging.

Owing to the Pareto frontier derived by CSA and MOPSO methods in the IEEE118-bus system is uneven and
has a strong discrete type, which are not compared in this part. The delightful thing is that the PF of IHCSA is well-distributed from Fig. 15, and its distribution has more significant advantages.

The BMS obtained by IHCSA, including active power loss of 54.3803 MW and basic fuel cost of $58513.8900 \$ / \mathrm{h}$, has obvious benefits over NSGA-II. TABLE XX reveals detailed comparison data.

TABLE XVIII depicts that the BMS gained by the proposed IHCSA approach has significant advantages.


Fig. 15. PFs of Case9

## 2) Case 10

In Case10, the $S_{\text {fcost }}$ and $S_{\text {emission }}$ are synchronously optimized by the proposed IHCSA and NSGA-II approaches to reflect the distinctions between the different methods.


Fig. 16. PFs of Case10
This case can thoroughly test the optimization ability of the above two methods in a large test system. To provide decision-makers with a practical reference value of an excellent control scheme.

Fig. 16 depicts that the PF of IHCSA is nearer to the real PF. Compared with NSGA-II, its distribution has significant advantages. The BMS obtained by IHCSA, including emission of $2.4463 \mathrm{ton} / \mathrm{h}$ and basic fuel cost of 61912.0100 $\$ / \mathrm{h}$, has obvious advantages over NSGA-II in TABLE XXI.

## VI. Performance Evaluation

In this paper, the PFs obtained by different algorithms are quantitatively analyzed by SP and HV. Meanwhile, eight optimization cases on IEEE30- and IEEE57-bus systems are

TABLE XX
DETAILS OF BMS FOR CASE9

| CS | IHCSA | NSGA-II | CS | IHCSA | NSGA-II |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{P}_{\text {Gen_4 }}(\mathrm{MW})$ | 5.0070 | 5.2445 | $\mathrm{V}_{\text {Gen_26 }}$ | 0.9979 | 1.0057 |
| $\mathrm{P}_{\text {Gen_6 }}$ | 5.0000 | 11.6364 | $\mathrm{V}_{\text {Gen_27 }}$ | 0.9975 | 1.0091 |
| $\mathrm{P}_{\text {Gen_8 }}$ | 5.0000 | 12.3650 | $\mathrm{V}_{\text {Gen_31 }}$ | 1.0018 | 1.0109 |
| $\mathrm{P}_{\text {Gen_10 }}$ | 202.9974 | 179.6695 | $\mathrm{V}_{\text {Gen_32 }}$ | 1.0295 | 0.9928 |
| $\mathrm{P}_{\text {Gen_12 }}$ | 244.3541 | 230.5180 | $\mathrm{V}_{\text {Gen_34 }}$ | 1.0333 | 0.9977 |
| $\mathrm{P}_{\text {Gen_15 }}$ | 18.4481 | 14.8453 | $\mathrm{V}_{\text {Gen_36 }}$ | 1.0247 | 0.9686 |
| $\mathrm{P}_{\text {Gen_18 }}$ | 68.6539 | 25.4540 | $\mathrm{V}_{\text {Gen_40 }}$ | 1.0212 | 0.9535 |
| $\mathrm{P}_{\text {Gen_19 }}$ | 15.1861 | 19.2120 | $\mathrm{V}_{\text {Gen_42 }}$ | 1.0006 | 1.0417 |
| $\mathrm{P}_{\text {Gen_24 }}$ | 5.7228 | 11.6513 | $\mathrm{V}_{\text {Gen_46 }}$ | 1.0291 | 1.0405 |
| $\mathrm{P}_{\text {Gen_25 }}$ | 100.6194 | 141.3584 | $\mathrm{V}_{\text {Gen_49 }}$ | 1.0393 | 1.0462 |
| $\mathrm{P}_{\text {Gen_26 }}$ | 277.6701 | 282.6833 | $\mathrm{V}_{\text {Gen_54 }}$ | 1.0409 | 1.0527 |
| $\mathrm{P}_{\text {Gen_27 }}$ | 8.0192 | 22.8670 | $\mathrm{V}_{\text {Gen_5 }}$ | 1.0385 | 1.0489 |
| $\mathrm{P}_{\text {Gen_31 }}$ | 8.0000 | 8.1908 | $\mathrm{V}_{\text {Gen_56 }}$ | 1.0315 | 1.0558 |
| $\mathrm{P}_{\text {Gen_32 }}$ | 64.7472 | 29.3844 | $\mathrm{V}_{\text {Gen_59 }}$ | 1.0230 | 1.0369 |
| $\mathrm{P}_{\text {Gen_34 }}$ | 8.9427 | 15.7024 | $\mathrm{V}_{\text {Gen_61 }}$ | 1.0210 | 1.0182 |
| $\mathrm{P}_{\text {Gen_36 }}$ | 53.9848 | 30.9166 | $\mathrm{V}_{\text {Gen_62 }}$ | 1.0240 | 1.0205 |
| $\mathrm{P}_{\text {Gen_40 }}$ | 8.0000 | 8.2890 | $\mathrm{V}_{\text {Gen_65 }}$ | 1.0336 | 1.0478 |
| $\mathrm{P}_{\text {Gen_42 }}$ | 8.3483 | 17.4059 | $\mathrm{V}_{\text {Gen_66 }}$ | 1.0352 | 1.0397 |
| $\mathrm{P}_{\text {Gen_46 }}$ | 29.6067 | 26.2924 | $\mathrm{V}_{\text {Gen_69 }}$ | 1.0103 | 1.0260 |
| $\mathrm{P}_{\text {Gen_49 }}$ | 250.0000 | 162.6309 | $\mathrm{V}_{\text {Gen_70 }}$ | 0.9936 | 0.9970 |
| $\mathrm{P}_{\text {Gen_54 }}$ | 185.6555 | 186.7033 | $\mathrm{V}_{\text {Gen_72 }}$ | 1.0165 | 1.0681 |
| $\mathrm{P}_{\text {Gen_5 }}$ | 64.5565 | 60.8435 | $\mathrm{V}_{\text {Gen_73 }}$ | 1.0008 | 0.9882 |
| $\mathrm{P}_{\text {Gen_56 }}$ | 42.9506 | 43.9825 | $\mathrm{V}_{\text {Gen_74 }}$ | 1.0099 | 1.0292 |
| $\mathrm{P}_{\text {Gen_59 }}$ | 87.6784 | 148.8000 | $\mathrm{V}_{\text {Gen_76 }}$ | 1.0201 | 1.0311 |
| $\mathrm{P}_{\text {Gen_61 }}$ | 107.8828 | 110.3558 | $\mathrm{V}_{\text {Gen_77 }}$ | 1.0259 | 1.0377 |
| $\mathrm{P}_{\text {Gen_62 }}$ | 25.0254 | 74.1492 | $\mathrm{V}_{\text {Gen_80 }}$ | 1.0023 | 1.0280 |
| $\mathrm{P}_{\text {Gen_65 }}$ | 287.1492 | 248.7397 | $\mathrm{V}_{\text {Gen_85 }}$ | 0.9845 | 0.9823 |
| $\mathrm{P}_{\text {Gen_66 }}$ | 266.7079 | 343.5521 | $\mathrm{V}_{\text {Gen_87 }}$ | 0.9734 | 0.9299 |
| $\mathrm{P}_{\text {Gen_69 }}$ | 37.0283 | 50.4957 | $\mathrm{V}_{\text {Gen_89 }}$ | 1.0089 | 1.0110 |
| $\mathrm{P}_{\text {Gen_70 }}$ | 10.0464 | 12.1782 | $\mathrm{V}_{\text {Gen_90 }}$ | 1.0120 | 1.0002 |
| $\mathrm{P}_{\text {Gen_72 }}$ | 6.1457 | 6.7566 | $\mathrm{V}_{\text {Gen_91 }}$ | 1.0195 | 0.9886 |
| $\mathrm{P}_{\text {Gen_73 }}$ | 5.3039 | 11.9832 | $\mathrm{V}_{\text {Gen_92 }}$ | 1.0088 | 1.0106 |
| $\mathrm{P}_{\text {Gen_74 }}$ | 77.0225 | 54.9103 | $\mathrm{V}_{\text {Gen_99 }}$ | 1.0291 | 0.9992 |
| $\mathrm{P}_{\text {Gen_76 }}$ | 25.0000 | 30.2879 | $\mathrm{V}_{\text {Gen_100 }}$ | 1.0033 | 1.0103 |
| $\mathrm{P}_{\text {Gen_77 }}$ | 189.3974 | 175.5451 | $\mathrm{V}_{\text {Gen_103 }}$ | 0.9760 | 1.0086 |
| $\mathrm{P}_{\text {Gen_80 }}$ | 28.3737 | 84.6949 | $\mathrm{V}_{\text {Gen_104 }}$ | 0.9923 | 1.0307 |
| $\mathrm{P}_{\text {Gen_85 }}$ | 10.0000 | 11.1145 | $\mathrm{V}_{\text {Gen_105 }}$ | 0.9992 | 1.0240 |
| $\mathrm{P}_{\text {Gen_87 }}$ | 142.1183 | 100.1340 | $\mathrm{V}_{\text {Gen_107 }}$ | 0.9811 | 0.9848 |
| $\mathrm{P}_{\text {Gen_89 }}$ | 50.9175 | 91.6709 | $\mathrm{V}_{\text {Gen_110 }}$ | 1.0326 | 0.9847 |
| $\mathrm{P}_{\text {Gen_90 }}$ | 8.0047 | 8.0766 | $\mathrm{V}_{\text {Gen_111 }}$ | 1.0343 | 1.0406 |
| $\mathrm{P}_{\text {Gen_91 }}$ | 20.6452 | 36.8795 | $\mathrm{V}_{\text {Gen_112 }}$ | 1.0384 | 0.9920 |
| $\mathrm{P}_{\text {Gen_92 }}$ | 105.3042 | 103.4046 | $\mathrm{V}_{\text {Gen_113 }}$ | 1.0173 | 1.0376 |
| $\mathrm{P}_{\text {Gen_99 }}$ | 100.0000 | 100.3301 | $\mathrm{V}_{\text {Gen_116 }}$ | 1.0279 | 1.0256 |
| $\mathrm{P}_{\text {Gen_100 }}$ | 144.3055 | 100.0000 | $\mathrm{T}_{8}$ (p.u.) | 0.9566 | 0.9125 |
| $\mathrm{P}_{\text {Gen_103 }}$ | 13.3264 | 16.7799 | $\mathrm{T}_{32}$ | 0.9424 | 1.0959 |
| $\mathrm{P}_{\text {Gen_104 }}$ | 25.4175 | 33.9713 | $\mathrm{T}_{36}$ | 0.9742 | 0.9269 |
| $\mathrm{P}_{\text {Gen_105 }}$ | 64.4166 | 30.5079 | $\mathrm{T}_{51}$ | 0.9757 | 0.9966 |
| $\mathrm{P}_{\text {Gen_107 }}$ | 13.5434 | 8.0083 | $\mathrm{T}_{93}$ | 0.9729 | 1.0445 |
| $\mathrm{P}_{\text {Gen_110 }}$ | 34.1036 | 31.5933 | $\mathrm{T}_{95}$ | 0.9922 | 0.9467 |
| $\mathrm{P}_{\text {Gen_111 }}$ | 25.0000 | 25.6738 | $\mathrm{T}_{102}$ | 0.9810 | 1.0700 |
| $\mathrm{P}_{\text {Gen_112 }}$ | 25.2142 | 25.0562 | $\mathrm{T}_{107}$ | 1.0204 | 1.0832 |
| $\mathrm{P}_{\text {Gen_113 }}$ | 28.0893 | 30.5120 | $\mathrm{T}_{127}$ | 1.0153 | 0.9838 |
| $\mathrm{P}_{\text {Gen_116 }}$ | 45.2644 | 29.2948 | $\mathrm{Q}_{\mathrm{C} 34}$ (p.u.) | 0.0135 | 0.2515 |
| $\mathrm{V}_{\text {Gen_1 }}($ p.u. $)$ | 0.9982 | 1.0612 | $\mathrm{Q}_{\mathrm{C} \text { _44 }}$ | 0.2674 | 0.1726 |
| $\mathrm{V}_{\text {Gen_4 }}$ | 0.9995 | 1.0571 | $\mathrm{Q}_{\mathrm{C} \text { _45 }}$ | 0.1380 | 0.1936 |
| $\mathrm{V}_{\text {Gen_6 }}$ | 0.9932 | 0.9714 | QC_46 | 0.1797 | 0.1473 |
| $\mathrm{V}_{\text {Gen_8 }}$ | 1.0255 | 0.9956 | $\mathrm{Q}_{\mathrm{C} \text { _48 }}$ | 0.2402 | 0.1688 |
| $\mathrm{V}_{\text {Gen_10 }}$ | 1.0018 | 1.0503 | $\mathrm{Q}_{\mathrm{C} \text { _74 }}$ | 0.1897 | 0.1611 |
| $\mathrm{V}_{\text {Gen_12 }}$ | 1.0184 | 1.0109 | $\mathrm{Q}_{\text {C_79 }}$ | 0.2443 | 0.1475 |
| $\mathrm{V}_{\text {Gen_15 }}$ | 1.0200 | 1.0371 | $\mathrm{Q}_{\mathrm{C} \text { _82 }}$ | 0.1783 | 0.2961 |
| $\mathrm{V}_{\text {Gen_18 }}$ | 1.0174 | 1.0156 | $\mathrm{Q}_{\mathrm{C} \text { _83 }}$ | 0.1182 | 0.0999 |
| $\mathrm{V}_{\text {Gen_19 }}$ | 1.0035 | 1.0301 | $\mathrm{Q}_{\mathrm{C} \text { _105 }}$ | 0.2050 | 0.2617 |
| $\mathrm{V}_{\text {Gen_24 }}$ | 0.9899 | 1.0170 | $\mathrm{Q}_{\mathrm{C} \text { _107 }}$ | 0.2013 | 0.2080 |
| $\mathrm{V}_{\text {Gen_25 }}$ | 1.0125 | 1.0835 | $\mathrm{Q}_{\mathrm{C} \text { _110 }}$ | 0.1381 | 0.0988 |
|  |  |  | $S_{\text {Ploss }}$ (MW) | 54.3803 | 56.8467 |
|  |  |  | $S_{\text {focost }}(\$ / \mathrm{h})$ | 58513.8900 | 59366.9100 |

## A. $S P$

The SP decipts the criterion deviation of two neighboring solutions in a set composed of mutually non-dominant solutions[28]. It can be described as (34).

$$
\begin{gather*}
S P=\sqrt{\sum_{i=1}^{n}\left(d_{\text {average }}-d_{i}\right)^{2}}  \tag{34}\\
d_{i}=\min _{o=1,2, \ldots, n}\left(\sum_{m=1}^{M}\left|f_{m}^{i}-f_{m}^{o}\right|\right) \tag{35}
\end{gather*}
$$

TABLE XXI
DETAILS OF BMS FOR CASE10

| CS | IHCSA | NSGA-II | CS | IHCSA | NSGA-II |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{P}_{\text {Gen_4 }}(\mathrm{MW})$ | 5.1230 | 7.1794 | $\mathrm{V}_{\text {Gen_26 }}$ | 1.0363 | 1.0732 |
| $\mathrm{P}_{\text {Gen_6 }}$ | 12.8263 | 10.8971 | $\mathrm{V}_{\text {Gen_27 }}$ | 0.9749 | 1.0234 |
| $\mathrm{P}_{\text {Gen_8 }}$ | 5.0000 | 11.1832 | $\mathrm{V}_{\text {Gen_31 }}$ | 0.9606 | 1.0040 |
| $\mathrm{P}_{\text {Gen_10 }}$ | 193.5924 | 284.9689 | $\mathrm{V}_{\text {Gen_32 }}$ | 0.9926 | 1.0464 |
| $\mathrm{P}_{\text {Gen_12 }}$ | 179.7772 | 201.4346 | $\mathrm{V}_{\text {Gen_34 }}$ | 0.9938 | 1.0412 |
| $\mathrm{P}_{\text {Gen_15 }}$ | 18.6344 | 11.9599 | $\mathrm{V}_{\text {Gen_36 }}$ | 0.9917 | 0.9990 |
| $\mathrm{P}_{\text {Gen_18 }}$ | 45.1393 | 46.0954 | $\mathrm{V}_{\text {Gen_40 }}$ | 1.0178 | 1.0318 |
| $\mathrm{P}_{\text {Gen_19 }}$ | 5.0000 | 16.6181 | $\mathrm{V}_{\text {Gen_42 }}$ | 1.0264 | 1.0004 |
| $\mathrm{P}_{\text {Gen_24 }}$ | 5.0000 | 5.4499 | $\mathrm{V}_{\text {Gen_46 }}$ | 1.0324 | 1.0218 |
| $\mathrm{P}_{\text {Gen_25 }}$ | 100.0000 | 101.3249 | $\mathrm{V}_{\text {Gen_49 }}$ | 1.0262 | 1.0102 |
| $\mathrm{P}_{\text {Gen_26 }}$ | 100.0000 | 121.9729 | $\mathrm{V}_{\text {Gen_54 }}$ | 1.0316 | 0.9913 |
| $\mathrm{P}_{\text {Gen_27 }}$ | 8.0000 | 28.6342 | $\mathrm{V}_{\text {Gen_5 }}$ | 1.0286 | 1.0085 |
| $\mathrm{P}_{\text {Gen_31 }}$ | 8.5877 | 18.4879 | $\mathrm{V}_{\text {Gen_56 }}$ | 1.0292 | 0.9530 |
| $\mathrm{P}_{\text {Gen_32 }}$ | 99.3617 | 42.3373 | $\mathrm{V}_{\text {Gen_59 }}$ | 0.9924 | 1.0294 |
| $\mathrm{P}_{\text {Gen_34 }}$ | 21.4048 | 23.9431 | $\mathrm{V}_{\text {Gen_61 }}$ | 1.0164 | 1.0315 |
| $\mathrm{P}_{\text {Gen_36 }}$ | 25.0000 | 25.2501 | $\mathrm{V}_{\text {Gen_62 }}$ | 1.0197 | 0.9947 |
| $\mathrm{P}_{\text {Gen_40 }}$ | 9.9399 | 15.0700 | $\mathrm{V}_{\text {Gen_65 }}$ | 1.0365 | 0.9683 |
| $\mathrm{P}_{\text {Gen_42 }}$ | 10.8984 | 8.0001 | $\mathrm{V}_{\text {Gen_66 }}$ | 0.9958 | 1.0880 |
| $\mathrm{P}_{\text {Gen_46 }}$ | 95.6233 | 90.9803 | $\mathrm{V}_{\text {Gen_69 }}$ | 0.9831 | 0.9720 |
| $\mathrm{P}_{\text {Gen_49 }}$ | 136.3450 | 247.0106 | $\mathrm{V}_{\text {Gen_70 }}$ | 0.9703 | 0.9407 |
| $\mathrm{P}_{\text {Gen_54 }}$ | 128.9885 | 121.6719 | $\mathrm{V}_{\text {Gen_72 }}$ | 1.0340 | 1.0447 |
| $\mathrm{P}_{\text {Gen_5 }}$ | 38.3923 | 64.4345 | $\mathrm{V}_{\text {Gen_73 }}$ | 0.9670 | 1.0425 |
| $\mathrm{P}_{\text {Gen_56 }}$ | 38.0486 | 30.1118 | $\mathrm{V}_{\text {Gen_74 }}$ | 1.0018 | 1.0219 |
| $\mathrm{P}_{\text {Gen_59 }}$ | 50.0000 | 50.8094 | $\mathrm{V}_{\text {Gen_76 }}$ | 1.0144 | 1.0239 |
| $\mathrm{P}_{\text {Gen_61 }}$ | 188.1862 | 89.9062 | $\mathrm{V}_{\text {Gen_77 }}$ | 0.9973 | 1.0062 |
| $\mathrm{P}_{\text {Gen_62 }}$ | 78.8032 | 46.8959 | $\mathrm{V}_{\text {Gen_80 }}$ | 1.0081 | 1.0179 |
| $\mathrm{P}_{\text {Gen_65 }}$ | 221.2279 | 363.5226 | $\mathrm{V}_{\text {Gen_85 }}$ | 0.9901 | 1.0352 |
| $\mathrm{P}_{\text {Gen_66 }}$ | 213.7170 | 150.6464 | $\mathrm{V}_{\text {Gen_87 }}$ | 1.0119 | 0.9514 |
| $\mathrm{P}_{\text {Gen_69 }}$ | 30.6825 | 30.7475 | $\mathrm{V}_{\text {Gen_89 }}$ | 1.0308 | 0.9962 |
| $\mathrm{P}_{\text {Gen_70 }}$ | 16.3638 | 13.6647 | $\mathrm{V}_{\text {Gen_90 }}$ | 1.0169 | 1.0456 |
| $\mathrm{P}_{\text {Gen_72 }}$ | 22.0174 | 20.3617 | $\mathrm{V}_{\text {Gen_91 }}$ | 1.0114 | 0.9773 |
| $\mathrm{P}_{\text {Gen_73 }}$ | 5.0183 | 20.0000 | $\mathrm{V}_{\text {Gen_92 }}$ | 1.0436 | 0.9959 |
| $\mathrm{P}_{\text {Gen_74 }}$ | 47.1793 | 34.1392 | $\mathrm{V}_{\text {Gen_99 }}$ | 1.0760 | 0.9765 |
| $\mathrm{P}_{\text {Gen_76 }}$ | 51.2797 | 40.6316 | $\mathrm{V}_{\text {Gen_100 }}$ | 1.0489 | 1.0317 |
| $\mathrm{P}_{\text {Gen_77 }}$ | 300.0000 | 164.8704 | $\mathrm{V}_{\text {Gen_103 }}$ | 1.0226 | 0.9530 |
| $\mathrm{P}_{\text {Gen_80 }}$ | 62.5641 | 32.9637 | $\mathrm{V}_{\text {Gen_104 }}$ | 1.0108 | 0.9456 |
| $\mathrm{P}_{\text {Gen_85 }}$ | 16.8765 | 23.5636 | $\mathrm{V}_{\text {Gen_105 }}$ | 1.0616 | 0.9694 |
| $\mathrm{P}_{\text {Gen_87 }}$ | 207.2688 | 208.6281 | $\mathrm{V}_{\text {Gen_107 }}$ | 1.0175 | 0.9307 |
| $\mathrm{P}_{\text {Gen_89 }}$ | 60.5256 | 72.2084 | $\mathrm{V}_{\text {Gen_110 }}$ | 1.0148 | 1.0016 |
| $\mathrm{P}_{\text {Gen_90 }}$ | 12.0636 | 10.3985 | $\mathrm{V}_{\text {Gen_111 }}$ | 1.0012 | 0.9786 |
| $\mathrm{P}_{\text {Gen_91 }}$ | 20.3372 | 24.7075 | $\mathrm{V}_{\text {Gen_112 }}$ | 0.9766 | 1.0385 |
| $\mathrm{P}_{\text {Gen_92 }}$ | 212.9350 | 142.1519 | $\mathrm{V}_{\text {Gen_113 }}$ | 1.0301 | 1.0022 |
| $\mathrm{P}_{\text {Gen_99 }}$ | 201.4881 | 183.9215 | $\mathrm{V}_{\text {Gen_116 }}$ | 0.9919 | 0.9728 |
| $\mathrm{P}_{\text {Gen_100 }}$ | 201.7482 | 250.0860 | $\mathrm{T}_{8}$ (p.u.) | 0.9677 | 1.0707 |
| $\mathrm{P}_{\text {Gen_103 }}$ | 13.0096 | 8.4881 | $\mathrm{T}_{32}$ | 0.9000 | 0.9692 |
| $\mathrm{P}_{\text {Gen_104 }}$ | 25.1885 | 25.2804 | $\mathrm{T}_{36}$ | 0.9675 | 0.9718 |
| $\mathrm{P}_{\text {Gen_105 }}$ | 25.0000 | 25.9516 | $\mathrm{T}_{51}$ | 1.0177 | 0.9118 |
| $\mathrm{P}_{\text {Gen_107 }}$ | 8.2824 | 13.4831 | $\mathrm{T}_{93}$ | 0.9720 | 1.0869 |
| $\mathrm{P}_{\text {Gen_110 }}$ | 35.0056 | 33.9498 | $\mathrm{T}_{95}$ | 1.0251 | 0.9338 |
| $\mathrm{P}_{\text {Gen_111 }}$ | 27.8755 | 30.7207 | $\mathrm{T}_{102}$ | 1.0396 | 0.9776 |
| $\mathrm{P}_{\text {Gen_112 }}$ | 47.9383 | 31.4164 | $\mathrm{T}_{107}$ | 0.9866 | 0.9769 |
| $\mathrm{P}_{\text {Gen_113 }}$ | 51.3876 | 43.5494 | $\mathrm{T}_{127}$ | 0.9871 | 0.9955 |
| $\mathrm{P}_{\text {Gen_116 }}$ | 36.9834 | 35.8061 | $\mathrm{Q}_{\mathrm{C} \_34}$ (p.u.) | 0.1356 | 0.2750 |
| $\mathrm{V}_{\text {Gen_1 }}(\mathrm{p} . \mathrm{u}$. | 1.0270 | 1.0154 | $\mathrm{Q}_{\mathrm{C} \text { _44 }}$ | 0.1989 | 0.2258 |
| $\mathrm{V}_{\text {Gen_4 }}$ | 1.0433 | 0.9871 | $\mathrm{Q}_{\mathrm{C} \text { _45 }}$ | 0.2651 | 0.0165 |
| $\mathrm{V}_{\text {Gen_6 }}$ | 0.9770 | 1.0575 | $\mathrm{Q}_{\mathrm{C} \text { _46 }}$ | 0.0577 | 0.2895 |
| $\mathrm{V}_{\text {Gen_8 }}$ | 0.9769 | 1.0783 | $\mathrm{Q}_{\mathrm{C} \text { _48 }}$ | 0.1747 | 0.1436 |
| $\mathrm{V}_{\text {Gen_10 }}$ | 0.9798 | 0.9818 | $\mathrm{Q}_{\mathrm{C} \text { _74 }}$ | 0.2755 | 0.0883 |
| $\mathrm{V}_{\text {Gen_12 }}$ | 1.0071 | 1.0045 | $\mathrm{Q}_{\mathrm{C} \text { _79 }}$ | 0.1532 | 0.1751 |
| $\mathrm{V}_{\text {Gen_15 }}$ | 1.0202 | 1.0723 | $\mathrm{Q}_{\mathrm{C} \text { _ } 82}$ | 0.1497 | 0.1252 |
| $\mathrm{V}_{\text {Gen_18 }}$ | 1.0075 | 1.0141 | $\mathrm{Q}_{\mathrm{C} \text { _83 }}$ | 0.2669 | 0.2266 |
| $\mathrm{V}_{\text {Gen_19 }}$ | 1.0171 | 1.0131 | Qc_105 | 0.0467 | 0.0452 |
| $\mathrm{V}_{\text {Gen_24 }}$ | 0.9646 | 0.9522 | Qc_107 | 0.2184 | 0.0081 |
| $\mathrm{V}_{\text {Gen_25 }}$ | 0.9453 | 0.9580 | $\mathrm{Q}_{\mathrm{C} \text { _110 }}$ | 0.1601 | 0.2947 |
|  |  |  | $S_{\text {emission }}(\mathrm{ton} / \mathrm{h})$ | 2.4463 | 2.5264 |
|  |  |  | $S_{\text {fcost }}(\$ / \mathrm{h})$ | 61912.0100 | 62160.8900 |

$$
\begin{equation*}
d_{\text {average }}=\frac{1}{n} \sum_{i}^{n} d_{i} \tag{36}
\end{equation*}
$$

where $d_{\text {average }}$, which has a practical reference point, denotes the mean value of all $d_{i}$.

## B. $H V$

HV is applied to calculate the super volume of the non-dominant solution set to the real Pareto frontier. Detailed descriptions of HV can be found in [24]. The wider the Pareto front is distributed, the larger the index, which indicates that the relative performance of the solution is better.

$$
\begin{equation*}
H V=C_{\text {volume }}\left(\bigcup_{i=1}^{\text {num }} v_{i}\right) \tag{37}
\end{equation*}
$$

where $v_{i}$ depicts the volume of the $i$ th individual with a fixed point.

## C. Statistical Analysis of Data

The analysis is anchored in 30 simulation tests of IHCSA, CSA, NSGA-II, and MOPSO algorithms.
The SP and HV will be calculated using the data from Case1-8. Besides, calculation results will be presented intuitively using the block diagram.

Box plots can reflect many characteristics of the data, including medians, outliers, etc.

The maximum and minimum data values are at the box's top and bottom, respectively. Meanwhile, the points scattered outside the box represent this data set's outliers. Fig. 17 reveals that the SP data of IHCSA fluctuates less. Compared with the other three algorithms, the average value of the data achieved by IHCSA is lower in most Cases. In Case 2 or Case 3, the SP data of IHCSA is slightly less volatile than the other three methods, but the average value of ones is smaller, and it has no outliers. From the simulation Cases, the Pareto front and BMS obtained by IHCSA are better than the other three algorithms.
Fig. 18 indicates that compared with the other three methods, the HV index of the data gained by IHCSA has less volatility. In most cases, the average value obtained by IHCSA is larger, and the deviation of data is minor. We can consider that the Pareto frontier obtained by this algorithm
has great diversity. TABLE XXII and TABLE XXIII depict detailed SP and HV indicators results.

## D. Algorithm Time Complexity

If an algorithm can find a quality solution, it requires to consume a lot of time as the cost. Combined, that means the method is not a valuable reference method. This paper uses the average running time to evaluate the time complexity of different algorithms. In practical problems, while an algorithm has excellent performance, the efficiency of solving the problem is also an essential factor for dispatchers to favor the algorithm. TABLE XXIV denotes the average running time of the four algorithms that ran 30 times independently in Case1-10. It is clear from Fig. 19 that compared with CSA, NSGA-II, and MOPSO, the IHCSA takes less time to solve MOOPF problems and is more likely to be favored by decision-makers, so it can be applied to practical engineering problems.

## VII. Conclusion

In this paper, a novel IHCSA method, which integrates sinusoidal nonlinear transformation awareness probability, tent map switching flight length, and cross mutation mechanism of DE algorithm, is proposed to deal with the MOOPF problem. Various multi-objective models are built up, considering $S_{\text {fcost }}, S_{V D}, S_{\text {fcost_ vp }}, S_{\text {emission }}$, and $S_{\text {Ploss }}$.

In the IEEE30-, IEEE57-, and IEEE118-bus test systems, ten cases that satisfy system constraints are applied to detect the applicability of IHCSA. Three multi-objective optimization strategies are combined: SAPM, ENSM, and BMS, to acquire a well-distributed Pareto frontier. Besides, time complexity and two performance evaluation indexes, SP and HV, are applied to test and evaluate the proposed algorithm's performance comprehensively. Through the experimental results, IHCSA has a tremendous advantage and strong competitiveness over MOPSO, CSA, and NSGA-II methods in processing the MOOPF problem.

Consequently, the proposed IHCSA is a selectable approach for treating the MOOPF problem in an actual power system.

TABLE XXII
DETAILS OF SP FOR VARIOUS METHODS

| Evaluation Index | Case | Mean $(M)$ and Deviation $(D)$ | Method |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | IHCSA | CSA | NSGA-II | MOPSO |
| SP | Case 1 | M | 0.8452 | 0.8042 | 0.8870 | 0.7860 |
|  |  | D | 0.0964 | 0.1234 | 0.0861 | 0.2418 |
|  | Case2 | M | 0.7591 | 0.8129 | 0.8198 | 0.6393 |
|  |  | D | 0.0902 | 0.0554 | 0.0600 | 0.2198 |
|  | Case3 | M | 0.9327 | 1.0227 | 1.0152 | 0.9231 |
|  |  | D | 0.0816 | 0.1067 | 0.1100 | 0.1472 |
|  | Case 4 | M | 0.0225 | 0.2558 | 0.0422 | - |
|  |  | D | 0.0215 | 0.3273 | 0.0209 | - ${ }^{-}$ |
|  | Case5 | M | 1.0405 | 1.0862 | 1.1284 | 0.8753 |
|  |  | D | 0.1224 | 0.1332 | 0.1869 | 0.2953 |
|  | Case6 | M | 0.0001 | 0.0059 | 0.0007 | 0.0015 |
|  |  | D | 0.0002 | 0.0061 | 0.0004 | 0.0012 |
|  | Case7 | M | 7.6493 | 25.4970 | 18.0732 | - |
|  |  | D | 14.1809 | 25.4946 | 5.2979 | - |
|  | Case8 | $M$ | 17.7315 | 58.6647 | 41.5369 | 105.8763 |
|  |  | D | 20.4094 | 41.7436 | 4.0056 | 61.6223 |




Fig. 18. Boxplots of HV for Case1-Case8

TABLE XXIII
DETAILS OF HV FOR VARIOUS METHODS

| Evaluation Index | Case | $\operatorname{Mean}(M)$ and Deviation $(D)$ | Method |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | IHCSA | CSA | NSGA-II | MOPSO |
| HV | Case 1 | M | 973.0801 | 930.2469 | 932.8931 | 834.0144 |
|  |  | D | 13.8670 | 31.9913 | 20.7314 | 216.8898 |
|  | Case2 | M | 30.7134 | 30.8212 | 30.9592 | 27.0245 |
|  |  | D | 0.41357 | 0.2781 | 0.3085 | 6.81304 |
|  | Case3 | M | 1501.1580 | 1472.8390 | 1484.9890 | 1414.0030 |
|  |  | D | 44.0461 | 32.71222 | 33.7807 | 95.6712 |
|  | Case4 | M | 262.4028 | 257.7612 | 266.4934 | - |
|  |  | D | 2.5497 | 5.0823 | 1.8411 | - |
|  | Case5 | M | 1027.1850 | 1015.7180 | 991.5192 | 805.9228 |
|  |  | D | 25.9278 | 25.3616 | 32.4580 | 195.7318 |
|  | Case6 | M | 0.2569 | 0.2005 | 0.2563 | 0.2610 |
|  |  | D | 0.0095 | 0.0572 | 0.0063 | 0.0054 |
|  | Case7 | M | 267013.5000 | 240781.1000 | 305393.4000 | - |
|  |  | D | 45366.8600 | 64731.4800 | 9425.8480 | - |
|  | Case8 | M | 52259.4200 | 48947.1500 | 59239.0900 | 57802.3000 |
|  |  | D | 7393.3220 | 12206.6900 | 348.4502 | 5374.7770 |

TABLE XXIV
THE MEAN ELAPSED TIME

| Method | The Mean Elapsed Time (s) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Case1 | Case2 | Case3 | Case4 | Case5 | Case6 | Case7 | Case8 | Case9 | Case10 |
| IHCSA | 198.7056 | 186.3052 | 189.8382 | 183.7133 | 210.4277 | 183.3281 | 442.5212 | 459.8592 | 1420.4730 | 1525.8020 |
| CSA | 198.3387 | 182.7500 | 195.4255 | 182.9518 | 208.5639 | 193.7357 | 491.5081 | 485.8934 | - | - |
| NSGA-II | 192.3326 | 185.1319 | 202.8209 | 189.5647 | 214.1398 | 204.3149 | 486.3406 | 529.6825 | 1555.6238 | 1485.0140 |
| MOPSO | 203.864 | 202.2720 | 196.8391 | - | 210.2265 | 231.6318 | 490.5029 | 502.7455 | - | - |



Fig. 19. The mean elapsed time of different algorithms

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